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ASX : FNT

ASX Limited Company Announcements Office Announcement

11th June 2014

10 Jackhammer Trenches Demonstrate a +215m Strike Length of Very High to Moderate Grade Gold in the Upper Zone - Swit Kia Prospect, with Excellent Strike/Dip/Plunge/Regional Structural Repetition Potential

Frontier Resources Ltd is very pleased to announce that the exploration program that targeted high grade gold mineralisation at the Bulago EL has returned very significant weighted average and individual assay intercepts from all 10 continuous Jackhammer trenches (of excavated, cleaned outcrop /creek exposures) in the Upper Zone at the Swit Kia Prospect (formerly Suguma), Papua New Guinea.

Very high grade gold mineralisation (>100 g/t) has been delineated at the Upper Zone (UZ) in silicified and altered intrusive, strongly brecciated and/or high sulphide rocks and at/near the intrusive /host siltstone contact. There were 13 different samples with >100 g/t gold, including a peak result with 1m grading 499 g/t gold.

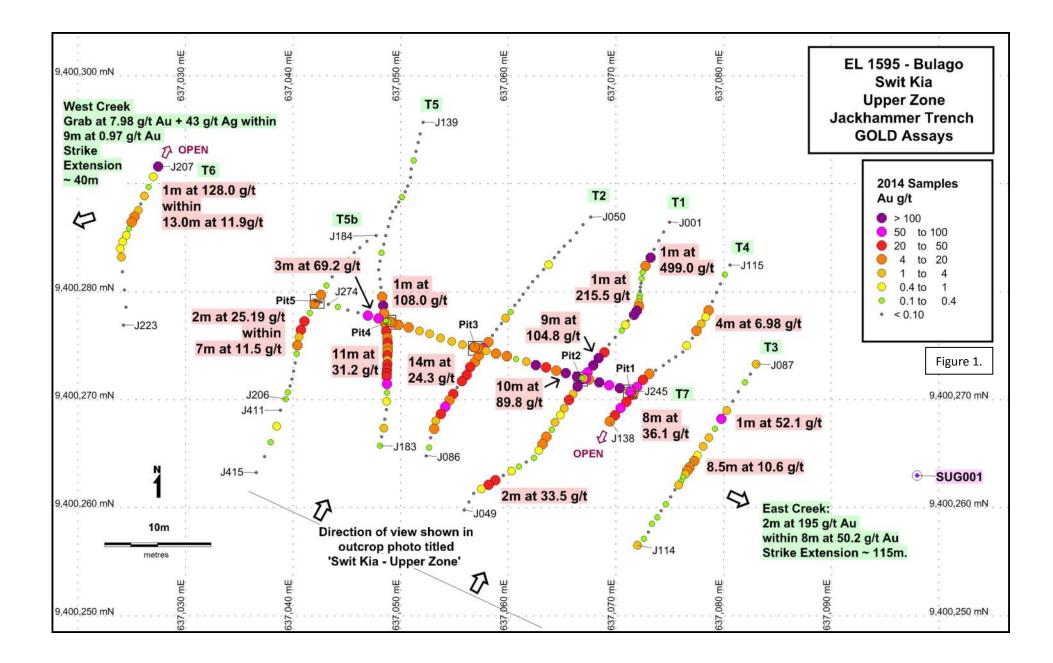
Significant jackhammer sample length assay highlights (that do not necessarily represent true lengths) in successive trenches from east to west (Figures 1 - 5) include:

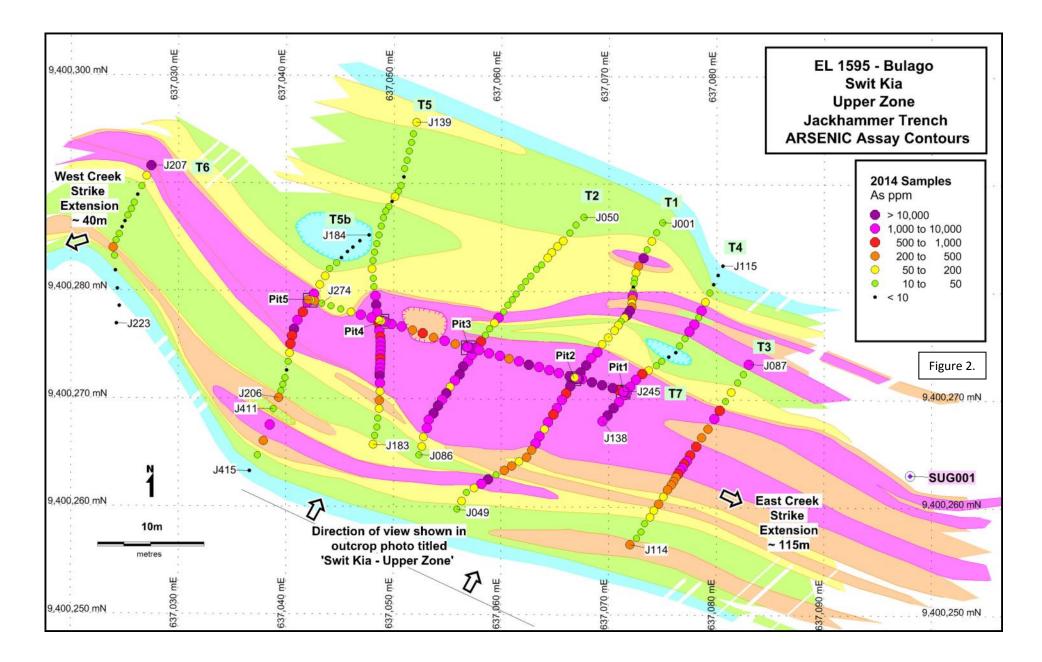
- **UZ** East Creek east bank with 2.0m grading 18.9 g/t gold (the only sample collected on the east bank)
- UZ East Creek west bank with 2.0m grading 195.0 g/t gold, within 8m grading 50.2 g/t gold (Figure 5)
- UZ -T3 with 2.0m grading 27.8 g/t gold, plus 5.5m of 3.07 g/t gold
- UZ -T4 with 8.0m grading 36.1 g/t gold, plus 4m of 6.98 g/t gold
- UZ -T1 with 2.0m grading 252.3 g/t gold, plus 1.5m grading 145.3 g/t gold, plus 5m grading 172.3 g/t gold, plus 14.0m grading 24.3 g/t gold
- UZ T2 with 1m grading 83.6 g/t gold, within 14m grading 24.3 g/t gold
- UZ T5 with 1m grading 108.5 g/t gold, within 11m grading 31.2 g/t gold
- UZ T5b with 2m grading 25.2 g/t gold, within 7m grading 11.5 g/t gold
- UZ -T6 with 1m grading 128.0 g/t gold, within 13m grading 11.9 g/t gold and
- UZ West Creek with a grab rock of 7.98 g/t gold, within 9m grading 0.97 g/t gold (gold grades are expected to improve as the intrusive contact is approached, as it was entirely within siltstone.

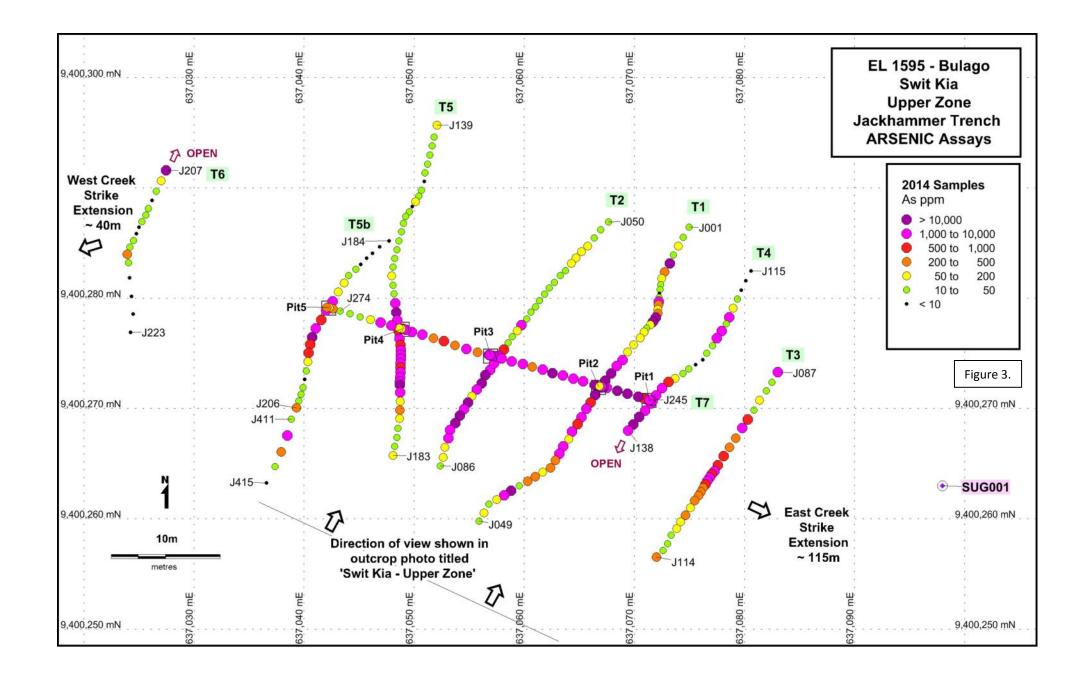
A composite total of 491.6m of sampling was completed in the Upper (410.3m) and Lower (81.3m) Zones and their strike extents (Refer to Appendix 1 for sample information and the plans/photos for location information).

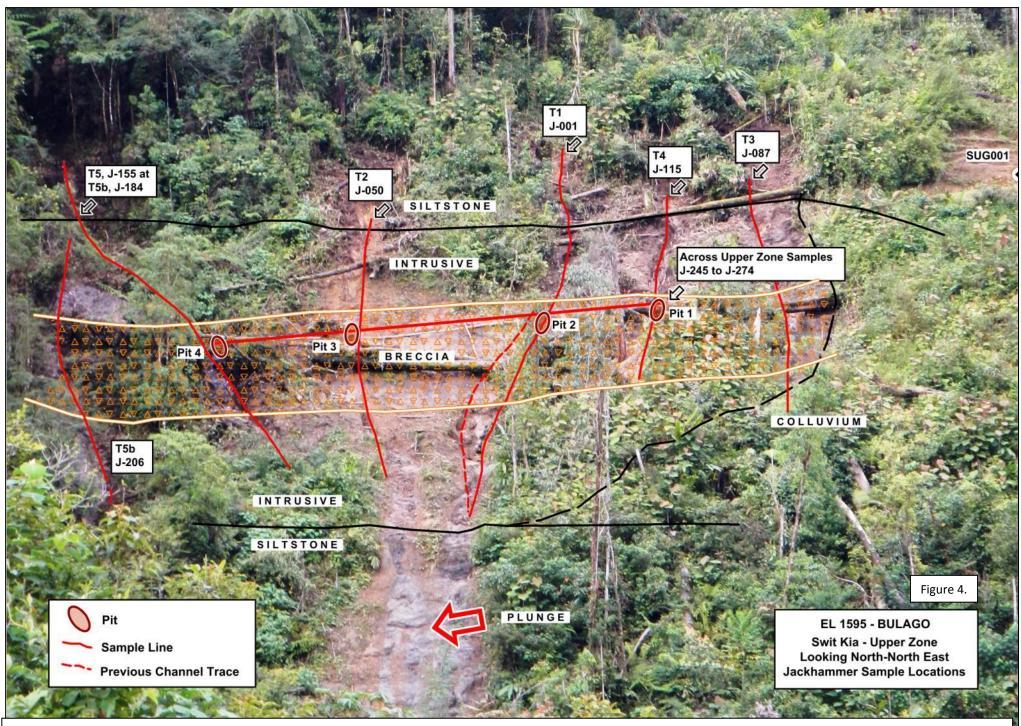
The Upper Zone discussed herein, was tracked and sampled in eight north - south trenches or mineralised outcrops over a 100m strike length, plus in one approx. east - west trending trench trending partly along strike. Another trench an additional 115m further east produced an excellent strike extension, to **total over 215 metres**.

The Lower Gold Zone at Swit Kia was also successfully prospected and rapidly sampled over +90m of approximately E-W strike length, while being explored as the 'secondary' target. It has an eastern strike extension (called East Creek breccia), that adds 90m, to make the total known and sampled strike length of the Lower Zone = 180m. Unfortunately the western extension (in West Creek) requires further cleaning to get to a lower RL where the higher grade mineralisation is expected to be located. The Lower Zone is viewed to have excellent gold mineralisation potential based on Frontier's late-2009 reconnaissance assays and recent geological evaluation. Assays from 2014 will be released when GIS drafting of the associated plans and review has been completed.









Upper Zone photograph looking more NNE (than the plans) showing jack-hammer trench sample locations, sample numbers and generalised lithologic units.

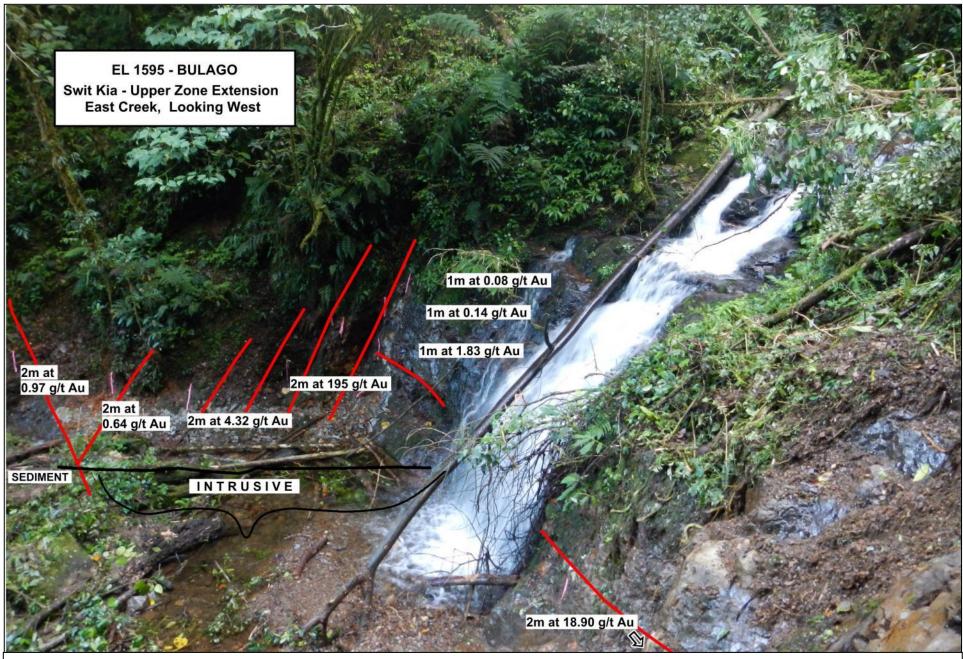


Figure 5. Upper Zone - East Creek 8.0m long trench on the west bank with intercepts of 2.0m grading 195.0 g/t gold, within 8.0m grading 50.2 g/t gold (402 grammetres gold) plus 2.0m grading 18.9 g/t gold as the only sample taken across the creek on the east bank (behind the photo). **Jack-Hammer Trench Assay Results.** The gold mineralised intercepts quoted below virtually cannot reflect true widths, as the geometry is uncertain and the samples were collected as possible 'down and/or across' the outcrops at least to some extent. The slope of the outcrop (E-W dip slope) is approximately 45 degrees, so if the mineralisation is sub-vertical or sub-horizontal and the then it would equate to about 70% of the 'down outcrop' length quoted. The true width of the mineralised zone is then related to the orientation of the sampling line and the strike of the gold mineralisation (best is perpendicular). The actual orientation of the gold mineralisation at the Swit Kia - Upper Zone is yet to be confirmed by specifically targeted drilling.

Weighted average 50 gram fire assay gold intercepts are noted below in order of the 'largest' amount of gold grading to the smallest amount. Table 1 follows it with the trenches in sequence from east to west and details of repeated 50 gram Fire, Gravimetric gold and silver- copper- zinc - lead - arsenic -antimony ICP assays.

All Upper Zone assays >0.10 g/t gold are included in Appendix 1, along with the gravimetric gold assays that were undertaken to check repeatability of high grade gold samples that contained high concentrations of arsenic. The gravimetric assays confirmed the Fire Assay results, with good repeatability and acceptable levels of variability, suggesting in future that only 50 gram Fire Assays are required.

UZ - T1 42.5m long trench approximately N-S down the outcrop with weighted internal intercepts of:

- 2.0m grading 252.3 g/t gold (505 gram-metres gold)
- Plus 1.5m grading 145.3 g/t gold (218 gram-metres gold)
- Plus 9.0m grading 104.8 g/t gold (943 gram-metres gold) incl 5m grading 172.3 g/t gold
- Plus 2.0m grading 10.6 g/t gold (21 gram-metres gold) followed by 6m of 0.27 g/t gold then
- Plus 2.0m grading 33.5 g/t gold (67 gram-metres gold).

The mineralised zone is 38.5m long down a small creek with a weighted average (no cutoff) of 45.8 g/t gold and peak gold of 1m grading 499 g/t, it contains a composite high grade weighted intercept of $\frac{20.5m \text{ grading } 85.6 \text{ g/t}}{\text{gold}}$ (for a composite total of $\frac{1,754}{1,754}$ gram-metres gold) and corresponding composite low tenor weighted intercept of 18m grading 0.43 g/t gold.

UZ - T7 30.0m long trench across the outcrop approximately E-W, with internal intercepts of:

26m grading 44.9 g/t gold (1,167 gram-metres gold) - entire trench consistently mineralised

- incl 10.0m grading 89.8 g/t gold (898 gram-metres gold) incl 1.0m grading 283.5 g/t gold
- Plus 13.0m grading 4.80 g/t gold (62 gram-metres gold)
- Plus 3.0m grading 69.2 g/t gold (208 gram-metres gold)
- for a composite total of <u>1,168</u> gram-metres gold.
- **UZ East** 8.0m long trench on the western bank of 'East Creek' with an intercept of:

2.0m grading 195.0 g/t gold, within 8.0m grading 50.2 g/t gold (402 gram-metres gold) and also 2.0m grading 18.9 g/t gold --- as the only sample taken across the creek on the eastern bank.

- UZ T2 37.0m long trench approximately N-S down the outcrop with an internal intercepts of:
 14.0m grading 24.3 g/t gold (339 gram-metres gold) including low internal interval-1m of 0.17 g/t gold.
- UZ T4 24.0m long trench approximately down the outcrop N-S with internal intercepts of: 8.0m grading 36.1 g/t gold (289 gram-metres gold)

Plus 4.0m grading 6.98 g/t gold (28 gram-metres gold)- incl 1.0m grading 17.8 g/t gold for a composite total of 317 gram-metres gold.

- **UZ T5** 40.0m long trench approximately down the outcrop N-S with an internal intercept of: 11.0m grading 31.2 g/t gold (343 gram-metres gold).
- **UZ T6** 21.0m long trench approximately N-S down outcrop in a creek with intercepts of: 13.0m grading 11.9 g/t gold (155 gram-metres gold)
- incl 1.0m grading 128.0 g/t gold
- and 2.0m grading 8.76 g/t gold
- and 5.0m grading 0.68 g/t gold

for a composite total of <u>176</u> gram-metres gold.

UZ - T5b 23.0m long trench N-S down outcrop with an intercept of 7.0m grading 11.5 g/t gold (80 gram-metres gold).

UZ - T3 24.0m long trench N-S down the outcrop with internal intercepts of:

2.0m grading 27.8 g/t gold (56 gram-metres gold)

Plus 5.5m grading 3.07 g/t gold (17 gram-metres gold)

for a composite total of <u>73</u> gram-metres gold.

UZ - W Ck 82.0m long trench ~N-S down 'West Creek' with an intercept in host siltstone rock only of: 9m grading 0.97 g/t gold, including 2.0m grading 2.86 g/t gold

for a composite total of ~9 gram-metres gold. A grab sample from this zone also returned 8.0 g/t gold.

Table 1.

| EL 1595 | i - Bula | igo Swit K | ia Prospect | Uppe | r Zone Tr | ench Ja | ckhamm | er Sampl | le Weigh | nted Ass | ays from | | West |
|----------------------|------------|-----------------------|-------------------------|---------------------------------|---------------------------|--------------|----------------|----------------|------------|----------------|------------|-----------|------------|
| Trench | | Intercept L | ength | Average Gold (Fire Assay) | Gold (gram/ metres) | Ag | Sample | Number | Cu | Zn | Pb | As | Sb |
| | | Down op/Trench | Estimated True Width | (g/t) | | (g/t) | From | То | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| | | 2.0 m | 1.6 m | 195.0 | 390 | 39.1 | | J-278 | 1,580 | 16,900 | 9,780 | 22400 | 19.2 |
| UZ E Ck N- W Bank | withi | 8.0 m | 6.4 m | 50.2 | 402 | 15.0 | J-278 | J-281 | 584 | 8,535 | 2,902 | 6161 | 20.8 |
| | Gram-ı | metres = | | | 390 | | | • | | | | | |
| E Ck N- W Ba | nk | 2.0 m | 1.6 m | 18.9 | 38 | 22.1 | | J-282 | 2,530 | 15,200 | 12,700 | 2230 | 16.0 |
| | | 2.0 m | 1.0 m | 27.8 | 56 | 7.6 | J-092 | J-093 | 346 | 209 | 1,843 | 2557 | 3.5 |
| UZ -T3 | PLUS | 5.5 m | 2.8 m | 3.07 | 17 | 2.4 | J-095 | J-102 | 88 | 1,352 | 534 | 1320 | 1.8 |
| | Cumula | ative Gram | -metres = | - | 73 | | | | - | | | | |
| | | 4.0 m | 2.0 m | 6.98 | 28 | 17.9 | J-120 | J-123 | 131 | 4,142 | 121 | 2417 | 3.3 |
| UZ -T4 | incl | 1.0 m | 0.5 m | 17.8 | 18 | 31.5 | | J-123 | 212 | 12,600 | 186 | 4030 | 6.0 |
| 02-14 | PLUS | 8.0 m | 4.0 m | 36.1 | 289 | | J-131 | J-138 | 293 | 948 | 999 | 8312 | 14.38 |
| | Cumula | ative Gram | -metres = | | 317 | | | | | | | | |
| | | 2.0 m | 1.0 m | 252.3 | 505 | 57.0 | J-005 | J-006 | 1,533 | 340 | 2,222 | 11030 | 19.0 |
| | PLUS | 1.5 m | 0.8 m | 145.3 | 218 | 40.9 | J-015 | J-017 | 517 | 5,220 | 3,441 | 23826 | 34.7 |
| | PLUS | 9.0 m | 4.5 m | 104.8 | 943 | 35.1 | J-024 | J-032 | 515 | 2,004 | 1,752 | 19292 | 39.0 |
| UZ -T1 | PLUS | 2.0 m | 1.0 m | 10.6 | 21 | 6.9 | J-036 | J-037 | 143 | 2,753 | 493 | 6780 | 19.0 |
| | PLUS | 2.0 m | 1.0 m | 33.5 | 67 | 7.9 | J-044 | J-045 | 112 | 515 | 451 | 11785 | 21.0 |
| | Cumula | ative Gram | -metres = | | 1,754 | | | | | | | | |
| | | 14.0 m | 7.0 m | 24.3 | 339 | 10.3 | J-070 | J-083 | 149 | 2,593 | 1,228 | 10497 | 20 |
| | incl | 7.0 m | 3.5 m | 25.1 | 176 | 13.7 | J-070 | J-076 | 176 | 3,541 | 1,669 | 7583 | 14.9 |
| UZ -T2 | PLUS | 6.0 m | 3.0 m | 27.3 | 164 | 7.8 | J-078 | J-083 | 133 | 1,690 | 872 | 15623 | 28.3 |
| | | ative Gram | | | 339 | | | 1 000 | 100 | 2,000 | 0/2 | 10020 | 2010 |
| | caman | 11.0 m | 5.5 m | 31.2 | 343 | 13.8 | J-161 | J-176 | 207 | 3,016 | 841 | 5969 | 9.6 |
| UZ -T5 | Gram | netres = | 5.5 11 | 51.2 | 343 | 15.0 | 5 101 | 5 170 | 207 | 3,010 | 041 | 5505 | 5.0 |
| | Grann- | 7.0 m | 3.5 m | 11.5 | 80 | 13.7 | J-193 | J-199 | 130 | 1,962 | 1,268 | 7695 | 17.1 |
| UZ -T5b | Gram | netres = | 3.5 11 | 11.5 | 80 | 13.7 | J-193 | J-199 | 130 | 1,902 | 1,208 | 7095 | 17.1 |
| | Grani- | 13.0 m | 6.5 m | 11.9 | 155 | 9.9 | J-207 | J-219 | 175 | 4 257 | 356 | 2092 | 5.2 |
| | inal | 13.0 m | 0.5 m | | | | J-207 | | | 4,357 | | | |
| UZ -T6 | incl | | | 128.0 | 128 18 | 31.3 | 1 313 | J-207 | 550 267 | 16,200 | 2,560 | 26500 | 64.0 |
| 02-10 | and and | 2.0 m 5.0 m | 1.0 m 2.5 m | 8.76 0.68 | 3 | 15.2 12.4 | J-213 J-215 | J-214 J-219 | 267 174 | 9,750 3,822 | 351 221 | 12 109 | 0.0 0.6 |
| | | ative Gram | | 0.68 | | 12.4 | J-215 | J-219 | 1/4 | 3,822 | 221 | 109 | 0.6 |
| | Cumula | | l . | 44.0 | 155 | 22.2 | 1.245 | 1 270 | 240 | 2.070 | 705 | 7670 | 14.2 |
| | in -1 | 26.0 m | 13.0 m | 44.9 | 1,167 | 22.2 | J-245 | J-270 | 248 | 2,878 | 785 | 7670 | 14.3 |
| | incl | 10.0 m | 5.0 m | 89.8 | 898 | 39.5 | J-245 | J-254 | 306 | 1,522 | 1,226 | 14961 | 25.8 |
| 117 77 5 117 | incl | 1.0 m | 0.5 m | 283.5 | 284 | 177.0 | 1 255 | J-254 | 795 | 1,760 | 3,730 | 33800 | 63.0 |
| UZ T7 E-W | and | 13.0 m | 6.5 m | 4.8 | 62 | 6.1 | J -255 | J-267 | 119 | 2,734 | 322 | 2467 | 8.8 |
| | and | 3.0 m | 1.5 m | 69.2 | 208 | 34.4 | J-268 | J-270 | 613 | 8,023 | 1,317 | 5917 | 15.3 |
| | | ative Gram | l . | 0.77 | 1,168 | | | | | | | | |
| | PLUS | 2.0 m | 1.0 m | 0.62 | 1.2 | 3.0 | | J-328 | 72 | 6,480 | 366 | 33 | 3.0 |
| | PLUS | 2.0 m | 1.0 m | 0.33 | 0.7 | 14.1 | | J-332 | 244 | 13,400 | 1,240 | 10 | - |
| West Creek | | 1.0 m | 0.5 m | 0.67 | 0.7 | 9.9 | | J-333 | 291 | 9,610 | 838 | 16 | - |
| | PLUS | 2.0 m | 1.0 m | 0.70 | 1.4 | 16.0 | | J-334 | 383 | 13,000 | 688 | 539 | - |
| | PLUS | 2.0 m | 1.0 m | 2.86 | 5.7 | 11.8 | | J-335 | 132 | 5,950 | 375 | 1540 | 9.0 |

Five shallow 'pits' or 'deeper impressions' (Table 2) were cut into the dip slope (with 20cm sample lengths), that showed the gold mineralised zone has variability (high to low gold grades) that may be relative to sample length and /or relative position in the mineralised zone. With high grades, this is expected and the pits didn't provide any additional idea of the depth extent of the mineralisation. The 4 x 25mm (1 inch) diameter and 800mm long hand holes that were drilled were unfortunately placed slightly above and missed the significantly gold mineralised horizon.

Geological modelling of the Swit Kia region shows a large number of factors interacting to localise gold mineralisation being:

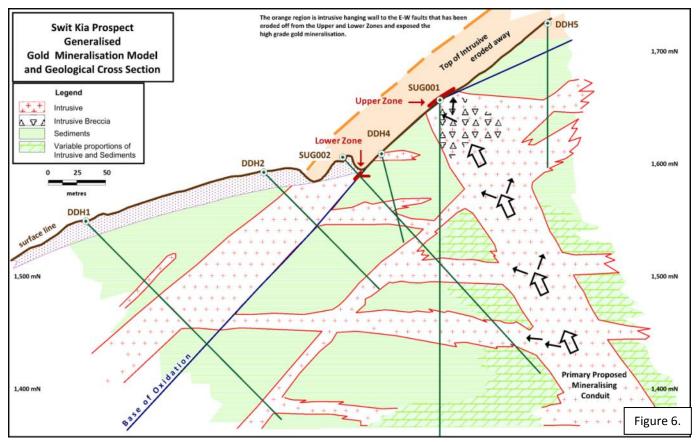
- 1. The Muller Anticline and the Bulago-Strickland Transfer Fault (at the regional scale), provided an excellent structural framework (flexing and faulting the sediments in various consistent orientations), that assisted in localising the 'recent' multi-phase intrusions and their gold and copper mineralisation.
- Mineralising fluids from the Bulago porphyry to the east and/or the Suguma porphyry to the west interacted in the Swit Kia region in dilational settings formed at the intersection of N-S and EW trending faults and also in proximal relatively flat lying but receptive host rocks.

| | | | | | | | | | ole z. |
|---------------|-----------------------------|-------|--------------------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Pit Number | Sample Number and Length | | Average FA 50 Gold (g/t) | Ag (g/t) | Cu (ppm) | Zn (ppm) | Pb (ppm) | As (ppm) | Sb (ppm) |
| | J-224 | 0.2 m | 18.70 | 4.3 | 130 | 1220 | 171 | 2180 | 14 |
| | J-225 | 0.2 m | 8.86 | 6.6 | 135 | 4100 | 655 | 4960 | 13 |
| 1 | J-226 | 0.2 m | 13.60 | 5.2 | 154 | 1650 | 663 | 5560 | 15 |
| | J-227 (| 0.2 m | 0.35 | 4.2 | 65 | 337 | 489 | 1030 | 5 |
| | J-228 | 0.2 m | 0.10 | 1.2 | 57 | 312 | 328 | 792 | 3 |
| | J-229 | 0.2 m | 58.60 | 14.3 | 253 | 4170 | 1830 | 20500 | 30 |
| 2 | J-230 | 0.2 m | 2.03 | 5.8 | 111 | 5990 | 540 | 1360 | 6 |
| 2 | J-231 | 0.2 m | 0.21 | 1.1 | 63 | 2680 | 141 | 131 | Х |
| | J-232 | 0.2 m | 0.17 | 3.1 | 74 | 2170 | 42 | 307 | Х |
| | J-233 | 0.2 m | 15.65 | 28.6 | 141 | 1690 | 338 | 6620 | 13 |
| 3 | J-234 | 0.2 m | 8.67 | 5.0 | 120 | 3790 | 278 | 2830 | 6 |
| 5 | J-235 | 0.2 m | 2.10 | 6.2 | 130 | 2740 | 507 | 2010 | 4 |
| | J -236 | 0.2 m | 4.42 | 13.1 | 142 | 4260 | 1520 | 3180 | 8 |
| | J-237 | 0.2 m | 6.72 | 9.8 | 146 | 1310 | 584 | 3700 | 5 |
| 4 | J-238 | 0.2 m | 5.69 | 3.2 | 105 | 1390 | 408 | 3960 | 6 |
| 4 | J-239 | 0.2 m | 0.26 | 6.4 | 86 | 2380 | 488 | 102 | Х |
| | J-240 | 0.2 m | 0.25 | 2.7 | 63 | 1660 | 462 | 126 | Х |
| | J-241 | 0.2 m | 0.04 | Х | 20 | 952 | 29 | 235 | Х |
| 5 | J-242 | 0.2 m | 0.03 | Х | 47 | 822 | 34 | 128 | Х |
| 5 | J-243 | 0.2 m | 0.03 | 0.6 | 42 | 1190 | 63 | 179 | Х |
| | J-244 | 0.2 m | 0.06 | 1.6 | 39 | 1070 | 89 | 264 | 3 |

- 3. A north dipping intrusive (that contains the consistently and strongly gold mineralised zone), with narrow very high gold grades localised mostly on its upper contact with the siltstone host.
- 4. Gold mineralised zones generally have strong to intense silicification and variable to intense brecciation and sulphide mineralisation (strong arsenic and variable zinc /silver association) and appear to be associated with the SW plunge and the dip slope (the E-W fault, not the N-S trending fault).
- 5. Conformable mineralisation in relatively flat lying sedimentary host rocks (that have specific layers more amenable to mineralising fluids) has been confirmed at the Lower Zone, but is inferred to be similar in the Upper Zone proximal to the dip slope, but obscured by the extensive brecciation.
- 6. Approximately E-W trending 'dip-slope' faults (dipping ~45° to S), with regional extent beyond EL boundaries.
- 7. Approximately N-S trending faults (dipping $\sim 45^{\circ}$ to W) with regional extent (refer to the photos in Appendix 1 to see photos of both types of structures and others).
- 8. Steeply dipping to sub-vertical faults and fractures zones occur in several orientations, often N and E-W trending (in the centre of the 'basin'), but perhaps post-mineralisation.
- 9. The intersection of the 45° dipping E-W and N-S trending faults produces a moderate to steep SW plunge. It is hypothesised that significant zones of brecciation and gold mineralisation are hosted down plunge and up/down dip at specific identifiable structural locations.

This structural setting/mineralising 'pattern' is repeated many times in the Bulago region and will be further investigated.

If you look at the cross section mineralisation model, it appears that drill hole SUG001 PRECLUDES mineralisation extending further to the east, but it is a 'matter of perspective or relative angle', as the dip slope mineralisation daylights (or is eroded off above the hole SUG001). As a comparison, think of the distortion of reality by looking at 2 fingers and rotating 90° until you only see one finger.



Chairman and Managing Director Peter McNeil M.Sc. commented: The exploration program at EL 1595 - Bulago Swit Kia Prospect Upper Zone was a resounding success with 10 excellent trench sampled assay intercepts from gold mineralised occurrences after we located, tracked laterally, cleaned, systematically jack-hammered (broken) into channels, sampled, mapped and evaluated them.

Trench 1 was sampled on a 1.0m and 0.5m down-outcrop basis and it has 5 zones for a cumulative total of 7m with >100 g/t gold (weighted average for the non-contiguous 5 zones =240 g/t gold). Trench 7 was slightly oblique to strike and it further defined the high grade zone with 10.0m grading 89.8 g/t gold (including 1.0m of 283.5 g/t) plus 3m of 69.2 g/t gold at its western end. The eastern outcrop strike extension of the Upper Zone returned 2m grading 195.0 g/t gold.

The very strongly brecciated and silica- sericite altered arsenopyrite- pyrite mineralised, E-W to ESE-WNW trending + moderate SW plunging zones are open along strike to the west and east and down dip/plunge.

The maximum strike length of the Upper Zone will be further defined with additional trenching in the eastern and western sectors of the Upper Zone to further demonstrate the continuity and grade of the high-grade gold mineralisation.

Frontier intends to demonstrate the dimensions of the high grade gold mineralisation at the Upper Zone of the Swit Kia Prospect, subject to completing a modest capital raising and when it is logistically possible. Cost effective drill testing is strongly warranted and Frontier can accomplish this task. Fortunately, enough diesel is already onsite at the Agali Airstrip residual from the OTML JV. One of the Company's small diamond core drilling rigs (that will drill to a maximum of 330m), drill gear, sampling and camp equipment is already containerised and ready to be shipped from Kimbe to Bulago.

The Landowners are pleased to have Frontier back exploring in their area and one of their two Spokesman (Andy Opene) last Friday informed me that since I left, their community has manually cut the grass for a proposed airstrip that is located much closer to the Swit Kia Prospect (and their village) than the present Agali Airstrip and importantly, without significant intervening topographic obstacles. Andy also noted that drainage ditches on the margins of the proposed airstrip will be completed this week. Frontier will seek approval for the airstrip from CASA when we resume exploration at Bulago for additional trenching and drilling and this should substantially lower our operational costs by rapidly eliminate the requirement for helicopter shuttles.

Comprehensive historic exploration information regarding Bulago was released to the ASX on 9/5/14, 1/4/14, 21/12/12, 18/10/12, 24/5/12, 17/5/12, 27/4/12, 28/2/11, 11/1/11, 15/1/10, 23/11/09, 11/9/09 & 2/9/2008 and for additional information relating to Frontier please visit our website at www.frontierresources.com.au

The Company has had email server issues for the last 3 months that have now been resolved and I apologise if any emails sent to <u>info@frontierresources.com.au</u> or web site applications to receive emails from Frontier have not been received, processed or responded to.

FRONTIER RESOURCES LTD

It MMil

P.A.McNeil, M.Sc., MAIG Chairman and Managing Director

Competent Person Statement:

The information in this report that relates to Exploration Results and Mineral Resources is based on information compiled by, or compiled under the supervision of Peter A. McNeil - Member of the Aust. Inst. of Geoscientists. Peter McNeil is the Managing Director of Frontier Resources, who consults to the Company. Peter McNeil has sufficient experience which is relevant to the type of mineralisation and type of deposit under consideration to qualify as Competent Person as defined in the 2012 Edition of the Australasian Code of Reporting Exploration Results, Mineral Resources and Ore Resources. Peter McNeil consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

APPENDIX 1. Photographs, Assay and Sample Tables



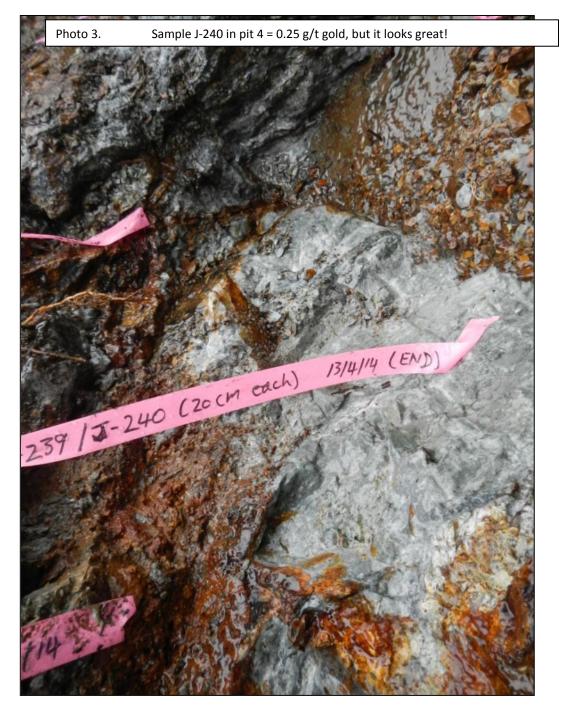


Photo 4. Sample J-031 from Trench 1, with 163.0 g/t gold in gravimetric analysis, but 38.0 g/t gold in 50 gram fire assay. This was the only significant 'anomaly' or difference between the 2 types of analyses.





Photo 5. Sample J-254 from Trench 7 with 283.5 g/t gold.



Photo 6. Sample J-246 from the start of Trench 7 (near Trench 4) with 156.0 g/t gold.

oto 7. Sample J-028 from Trench 1 with 222.0 g/t gold, crossing near Trench 7 mple J-250, with 155.5 g/t gold.

Photo 8. Pit 1 showing samples J-224-228 (18.70 to 0.10 g/t gold) and an apparent shallow SW plunge (to the left).



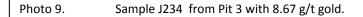




Photo 10. Grab Sample G002 - a magnificent hydrothermal breccia in siltstone from East Creek (with only 7.98 g/t gold + 43.2 g/t silver), that documents the western strike extension of the Upper Zone. More intensely mineralised intrusive is likely to be very nearby subsurface based on the mineralisation model.



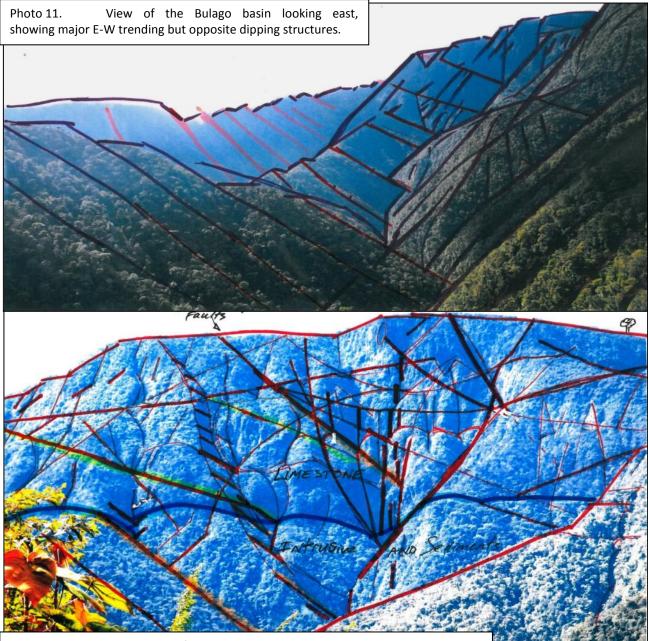
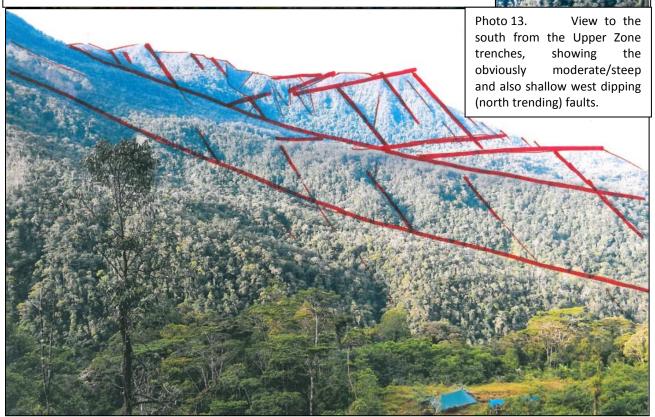


Photo 12. A close up of a similar easterly view as above, also showing the limestone-intrusive/sediment contact..



| EL 1595 - Bulago Swit Kia Propsect Jackhammer Trenching | | | | | | | | | | |
|--|-------------------------|-----------------------|----------------|--|--|--|--|--|--|--|
| Trench or pit Number | Sample Number (From) | Sample Number (To) | Length | | | | | | | |
| 1 | J-001 | J-049 | 42.5 m | | | | | | | |
| 2 | J-050 | J-086 | 37.0 m | | | | | | | |
| 3 | J-087 | J-114 | 24.0 m | | | | | | | |
| 4 | J-115 | J-138 | 24.0 m | | | | | | | |
| 5 | J-139 | J-183 | 40.0 m | | | | | | | |
| 5b | J-184 | J-206 | 23.0 m | | | | | | | |
| 6 | J-207 | J-223 | 21.0 m | | | | | | | |
| Pit 1 | J-224 | J-228 | 1.0 m | | | | | | | |
| Pit 2 | J-229 | J-232 | 0.8 m | | | | | | | |
| Pit 3 | J-233 | J -236 | 0.8 m | | | | | | | |
| Pit 4 | J-237 | J-240 | 0.8 m | | | | | | | |
| Pit 5 | J-241 | J-244 | 0.8 m | | | | | | | |
| 7 E-W | J-245 | J-274 | 30.0 m | | | | | | | |
| E ck N -W | J-277 | J-281 | 9.0 m | | | | | | | |
| Eck N - E | | J-282 | 2.0 m | | | | | | | |
| E Ck Central | J-283 | J-292 | 10.0 m | | | | | | | |
| E Ck Central | J-293 | J-297 | 10.0 m | | | | | | | |
| E Ck S Bx | J-298 | J-300 | 6.0 m | | | | | | | |
| E Ck S Bx | J-301 | J-308 | 12.0 m | | | | | | | |
| 14 | | J-309 | 1.0 m | | | | | | | |
| | J-310 | J-310 | 1.0 m | | | | | | | |
| | J-311 | J-311 | 1.0 m | | | | | | | |
| East C reek | J-312 | J-312 | 1.8 m | | | | | | | |
| Fault | J-313 | J-313 | 1.0 m | | | | | | | |
| | J-314 | J-314 | 0.8 m | | | | | | | |
| | J-315 | J-315 | 1.0 m | | | | | | | |
| West Ck | J-316 | J-357 | 82.0 m | | | | | | | |
| Mid Ck UZ ex | J-358 | J-365 | 16.0 m | | | | | | | |
| LZ | | J-366 | 0.7 m | | | | | | | |
| Central Ck | J-367 | J-372 | 23.9 m | | | | | | | |
| LZ - 3 | J-373 | J-379 | 6.3 m | | | | | | | |
| LZ - 2 | J-380 | J-387 | 8.0 m | | | | | | | |
| LZ - 4 | J-388 | J-399 | 11.4 m | | | | | | | |
| | | J-400 | 0.3 m | | | | | | | |
| LZ - 5 | | J-401 | 0.3 m | | | | | | | |
| 17.0 | 1.402 | J-402 | 1.0 m | | | | | | | |
| LZ -6 | J-403 | J-404 | 4.0 m | | | | | | | |
| LZ - W Ck | J-405 | J-406 | 4.7 m | | | | | | | |
| | | J-407 | 2.0 m | | | | | | | |
| LZ - W Ck | | J-408 | 1.0 m | | | | | | | |
| | | J-409 | 1.5 m | | | | | | | |
| | | J-410 | 2.0 m | | | | | | | |
| UZ 5b Ext | J-411 | J-415 | 10.0 m | | | | | | | |
| LZ East ext | | J-416 | 0.4 m | | | | | | | |
| LZ - 7 | J-417 | J-421 | 5.3 m | | | | | | | |
| | 1 4 2 2 | J-422 | 1.0 m | | | | | | | |
| LZ - 8 | J-423 | J-427 | 5.0 m | | | | | | | |
| LZ East ext | | J-428 J-429 | 1.0 m 1.5 m | | | | | | | |
| | | | | | | | | | | |
| | | Total= | 491.6 m | | | | | | | |

| Sample Number | Average Gold | Gold (Gravimetric) | Gold (FA 50) | Gold (FA 50) | Gold (FA 50) | Gold (FA 50) | Ag | Cu (nnm) | Zn (nnm) | Pb (nnm) | As (nnm) | Sb (nnm) | | · · · · | Number | Average Gold | Gold (Gravimetric) | Gold (FA 50) | Gold (FA 50) | Gold (FA 50) | Gold (FA 50) | Ag (g/t) | Cu (nnm) | Zn (nnm) | Pb (nnm) | As (ppm) | Sb (nnm) |
|---|--------------------------------------|--------------------------------|---------------------------------------|------------------|-------------------------|-----------------|------------------------------|--------------------|-----------------------|---------------------|------------------------------|----------------|------------|----------------------|-------------------------|------------------------------|--------------------------|------------------------------|---------------------|-------------------|-----------------|-----------------------------|--------------------|-----------------------|---------------------------|---------------------------|---------------------|
| and Length | (FA50 - g/t) 499.00 | (g/t) | (g/t) 499.00 | (g/t) | (g/t) - | (g/t) - | (g/t) 114.0 | (ppm) 2980 | (ppm) 285 | (ppm) 4340 | 21600 | (ppm) 38 | J- | | 1.0 m | (FA50 - g/t) 0.11 | (g/t) | (g/t) | (g/t) - | (g/t) - | (g/t) - | (g/t) X | 34 | 72 | (ppm) 11 | 68 | (ppm) |
| J-006 1.0 m J-007 1.0 m J-008 0.5 m | 5.66 0.25 0.29 | - | 5.66 0.25 0.29 | - | - | - | X X X | 86 21 23 | 395 335 335 | 103 47 20 | 460 113 27 | X X X | J- | -193 -194 -195 | 1.0 m 1.0 m 1.0 m | 9.28 5.28 0.18 | - | 9.28 5.28 0.18 | - | - | - | 5.5 7.6 2.5 | 103 71 75 | 1100 978 331 | 773 211 138 | 5320 2660 545 | <u>11</u> 6 2 |
| J-012 0.5 m J-013 0.5 m | 0.37 | - | 0.37 | - | - | - | 1.9 1.1 | 72 60 | 1190 1270 | 105 56 | 3990 374 | 5 X | J- | -196 -197 | 1.0 m 1.0 m | 22.37 28.00 | 27.80 30.60 | 20.00 | 22.37 - | 22.00 | 25.10 | 11.5 14.8 | 139 337 | 1760 3750 | 716 4300 | 9340 34100 | 26 72 |
| J-014 0.5 m J-015 0.5 m | 1.40 4.34 | - | 1.46 4.34 | 1.40 - | <u>1.34</u> | - | X 13.2 | 49 121 | 1790 7940 | 368 184 | 121 377 | X X | J- | -198 -199 | 1.0 m 1.0 m | 1.95 13.20 | - | 1.95 13.20 | - | - | - | 48.6 5.7 | 113 72 | 4860 955 | 2590 145 | 955 945 | X 3 |
| J-016 0.5 m J-017 0.5 m | 317.50 114.00 | 303.00 139.00 | 284.00 114.00 | | 351.00 | - | 87.7 21.9 | 1020 411 | 4770 2950 | 7390 2750 | 46600 24500 | 72 32 | | -200 -205 | 1.0 m 1.0 m | 0.17 | - | 0.17 | - | - | - | 0.9 0.9 | 28 76 | 909 1210 | 42 31 | 164 46 | X X |
| J-020 0.5 m J-021 1.0 m | 0.54 | - | 0.54 | - | - | - | X | 27 43 | 435 438 | 17 20 | 77 116 | X X | J- | -206 -207 | 1.0 m 1.0 m | 0.12 | 120.00 | 0.12 | | 131.00 | | 1.0 31.3 | 53 550 | 129 16200 | 20 2560 | 380 26500 | X 64 |
| J-024 1.0 m J-025 1.0 m J-026 1.0 m | 39.53 320.00 120.00 | | 38.00 319.00 120.00 | - | 36.10 321.00 | 44.50 | 17.7 102.0 31.9 | 261 2650 778 | 311 3180 1890 | 374 3930 2120 | 2290 2910 41400 | 8 50 64 | J- | -208 -209 -210 | 1.0 m 1.0 m 1.0 m | 0.48 0.15 3.04 | - | 0.48 0.15 3.04 | · · | - | - | 0.9 1.6 0.8 | 87 87 51 | 204 507 424 | 22 86 77 | 70 27 9 | X X X |
| J-027 1.0 m J-028 1.0 m | 53.80 222.00 | 51.00 194.00 | 54.00 222.00 | 53.80 | 53.60 | - | 26.5 83.8 | 284 321 | 2010 2310 | 1760 2580 | 24200 79800 | 50 140 | J- | -212 -213 | 1.0 m 1.0 m | 1.43 12.20 | - | 1.43 12.20 | - | - | - | 1.6 22.4 | 74 358 | 452 13700 | 60 457 | 11 23 | X X X |
| J-029 1.0 m J-030 1.0 m | 145.50 2.03 | 239.00 | 161.00 2.03 | 145.50 - | 130.00 - | - | 38.0 6.7 | 239 92 | 1440 4380 | 2520 180 | 16700 939 | 26 2 | | -214 -215 | 1.0 m 1.0 m | 5.32 0.24 | - | 5.32 0.24 | - 0.24 | - | - 0.23 | 7.9 4.3 | 176 94 | 5800 3620 | 245 68 | X X | X X |
| J-031 1.0 m J-032 1.0 m | 38.00 2.16 | <u>163.00</u> | 38.00 2.16 | - | - | - | 6.4 2.8 | 194 79 | 2600 228 | 1480 1200 | 6670 1010 | <u>14</u> 5 | J- | -216 -217 | 1.0 m 1.0 m | 0.46 0.99 | - | 0.46 | - | - | - | 4.5 22.1 | 168 308 | 1840 6750 | 85 246 | 11 16 | X X |
| J-033 1.0 m J-034 1.0 m J-035 1.0 m | 0.50 3.37 0.11 | - | 0.50 3.54 0.11 | - 3.37 | 3.20 | - | 2.8 10.0 0.6 | 88 142 61 | 376 1110 352 | 488 954 108 | 641 2880 119 | 3 7 X | J- | -218 -219 -224 | 1.0 m 1.0 m 0.2 m | 0.58 1.12 18.70 | - | 0.58 1.12 18.70 | 0.58 - | 0.57 - | - | 7.6 23.5 4.3 | 188 110 130 | 1690 5210 1220 | 296 411 171 | 496 23 2180 | 3 X 14 |
| J-036 1.0 m J-037 1.0 m | 13.50 7.68 | 14.90 8.50 | 13.50 7.68 | - | - | - | 6.3 7.4 | 171 115 | 4620 886 | 546 440 | 5900 7660 | 17 21 | J-, | -225 | 0.2 m 0.2 m | 8.86 13.60 | - | 8.86 13.60 | - | - | - | 6.6 5.2 | 135 135 154 | 4100 1650 | 655 663 | 4960 5560 | 13 15 |
| J-038 1.0 m J-039 1.0 m | 0.52 0.26 | - | 0.52 0.26 | - | - | - | 4.8 X | 47 25 | 577 388 | 945 60 | 338 277 | X X | | -227 -228 | 0.2 m 0.2 m | 0.35 0.10 | - | 0.35 0.10 | - | - | - | 4.2 1.2 | 65 57 | 337 312 | 489 328 | 1030 792 | 5 3 |
| J-041 1.0 m J-042 1.0 m | 0.31 | - | 0.31 | - | - | - | X X | 36 55 | 816 1290 | 42 30 | 201 427 | 2 X | J-, | -229 -230 | 0.2 m 0.2 m | 58.60 2.03 | 49.30 - | 59.50 2.03 | 58.60 - | 57.70 - | - | 14.3 5.8 | 253 111 | 4170 5990 | 1830 540 | 20500 1360 | 30 6 |
| J-044 1.0 m J-045 1.0 m | 34.70 32.25 0.44 | 36.60 36.70 | 30.60 32.70 0.44 | 34.70 32.25 | 38.80 31.80 | - | 8.3 7.5 0.5 | 87 136 83 | 437 592 87 | 625 277 35 | 17600 5970 56 | 31 11 X | J-, | -231 -232 | 0.2 m 0.2 m | 0.21 0.17 15.65 | - | 0.21 0.17 15.50 | - - 15.65 | - - 15.80 | - | 1.1 3.1 28.6 | 63 74 141 | 2680 2170 1690 | 141 42 338 | 131 307 6620 | X X 13 |
| J-046 1.0 m J-057 1.0 m J-065 1.0 m | 0.44 0.46 0.16 | - | 0.44 0.46 0.16 | - | - | - | 0.5 2.4 0.8 | 83 64 32 | 87 224 276 | 35 57 14 | 18 18 | X X X | J-, | -233 -234 -235 | 0.2 m 0.2 m 0.2 m | 8.67 2.10 | - | 8.75 2.10 | 15.65 8.67 - | - | - 8.58 - | 28.6 5.0 6.2 | 141 120 130 | 1690 3790 2740 | 338 278 507 | 2830 2010 | 13 6 4 |
| J-066 1.0 m J-070 1.0 m | 1.20 4.42 | - | 1.20 4.42 | - | - | - | 1.3 1.9 | 79 85 | 217 217 1250 | 14 115 182 | 1170 993 | 3 X | J- | -235 -236 -237 | 0.2 m 0.2 m 0.2 m | 4.42 6.72 | - | 4.42 6.72 | - | - | - | 0.2 13.1 9.8 | 130 142 146 | 4260 1310 | 1520 584 | 3180 3700 | 8 5 |
| J-071 1.0 m J-072 1.0 m | 62.25 5.88 | 51.50 - | 58.20 5.88 | 62.25 | 66.30 - | - | 30.3 13.4 | 163 165 | 3810 3550 | 149 1270 | 1110 2490 | 7 9 | J-, | -238 -239 | 0.2 m 0.2 m | 5.69 0.26 | - | 5.69 0.23 | - 0.26 | - 0.29 | - | 3.2 6.4 | 105 86 | 1390 2380 | 408 488 | 3960 102 | <mark>6</mark> Х |
| J-073 1.0 m J-074 1.0 m | 13.80 27.55 | 25.80 | 13.80 29.70 | 27.55 | 25.40 | - | 10.7 20.5 | 206 309 | 5710 4720 | 4500 3570 | 4940 21000 | 11 41 | J- | -240 -245 | 0.2 m 1.0 m | 0.25 55.30 | - | 0.25 55.30 | - | - | - | 2.7 15.8 | 63 175 | 1660 882 | 462 568 | 126 2280 | X 11 |
| J-075 1.0 m J-076 1.0 m J-077 1.0 m | 33.90 27.80 0.17 | 34.00 | 32.20 29.40 | 33.90 27.80 | 35.60 26.20 | - | 5.8 13.3 1.6 | 127 175 59 | 1890 3860 1370 | 1400 611 284 | 20800 1750 136 | 36 X X | J-, | -246 -247 -248 | 1.0 m 1.0 m | 156.00 72.07 19.45 | 205.00 69.10 33.10 | 156.00 68.80 19.80 | - 72.07 19.45 | 80.40 19.10 | - 67.00 | 119.0 22.4 2.7 | 736 378 119 | 2150 1540 1080 | 1100 871 480 | 20600 16900 12500 | 43 25 14 |
| J-077 1.0 m J-078 1.0 m J-079 1.0 m | 38.60 4.46 | 44.50 | 35.80 4.46 | 38.60 | 41.40 | - | 4.9 2.6 | 245 71 | 1370 1850 732 | 1630 192 | 33400 1180 | 68 6 | J-, | -248 -249 -250 | 1.0 m 1.0 m 1.0 m | 6.70 155.50 | - 182.00 | 6.70 137.00 | - | - 174.00 | - | 1.7 34.5 | 119 120 241 | 2050 1560 | 345 1130 | 3460 46700 | 6 6 |
| J-080 1.0 m J-081 1.0 m | 83.60 28.15 | 86.10 33.80 | 74.80 27.50 | 83.60 28.15 | 92.40 | 28.80 | 25.1 5.8 | 149 95 | 2070 836 | 1200 784 | 26000 26900 | 42 39 | J-, | -251 -252 | 1.0 m 1.0 m | 106.90 9.11 | - | 95.80 9.11 | - | 118.00 | - | 10.6 2.1 | 214 68 | 1560 562 | 1170 427 | 9230 1410 | 19 4 |
| J-082 1.0 m J-083 1.0 m | 3.24 5.80 | - | 3.24 5.80 | - | - | - | 1.6 6.8 | 78 162 | 1210 3440 | 194 1230 | 2230 4030 | 5 10 | J-, | -253 -254 | 1.0 m 1.0 m | 33.20 283.50 | <u>-</u> 257.00 | 29.90 280.00 | 33.20 283.50 | _ 287.00 | 36.50 | 9.5 177.0 | 214 795 | 2080 1760 | 2440 3730 | 2730 33800 | 7 63 |
| J-085 1.0 m J-087 1.0 m | 0.20 1.70 | - | 0.20 1.70 0.13 | - | - | - | X 1.2 | 43 57 27 | 151 671 | 11 341 | 81 1070 | X X | J- | -255 -256 | 1.0 m 1.0 m | 2.65 0.13 | - | 2.65 0.13 | - | - | - | 8.6 0.6 | 146 72 | 1730 541 | 303 88 | 1580 361 | 5 X |
| J-089 1.0 m J-092 1.0 m J-093 1.0 m | 0.13 3.53 52.10 | 37.60 | 3.53 47.40 | - | 56.80 | - | X 1.3 13.8 | 99 593 | 287 116 301 | 14 535 3150 | 40 583 4530 | X X 7 | J- | -257 -258 -259 | 1.0 m 1.0 m 1.0 m | 6.22 7.71 2.63 | - 12.10 - | 6.22 7.71 2.63 | - | - | - | 4.6 4.8 4.2 | 103 217 113 | 921 1080 1290 | 520 434 516 | 7250 9570 2650 | 10 16 3 |
| J-094 1.0 m J-095 1.0 m | 0.15 | - | 0.15 | - | - | - | 1.1 | 95 46 | 250 316 | 659 38 | 291 263 | _ | J- | | 1.0 m 1.0 m | 8.70 3.13 | - 6.60 | 8.70 3.13 | - | - | - | 4.6 12.5 | 102 132 | 2150 4500 | 374 323 | 2390 316 | 8 X |
| J-096 1.0 m J-097 1.0 m | 1.11 0.75 | - - | 1.11 0.75 | - | - | - | | 45 52 | 366 305 | 56 30 | 757 746 | | | -262 -263 | 1.0 m 1.0 m | 1.81 3.37 | - | 1.81 3.37 | - | - | - | 2.6 9.5 | 85 122 | 2220 7620 | 292 245 | 1440 314 | 5 3 |
| J-098 0.5 m J-099 0.5 m | 6.08 0.29 | 7.60 - | 6.08 0.29 | - | - | - | 4.0 7.8 | 221 | 470 464 | 504 1500 | 5030 756 | 5 | J- | -264 -265 | 1.0 m 1.0 m | 2.07 | - | 1.85 1.01 | 2.07 | <u>2.29</u> - | - | 2.9 3.6 | 62 83 | 1710 2690 | 114 88 | 524 200 | X 3 |
| J-100 0.5 m J-101 0.5 m J-102 0.5 m | 4.29 15.70 1.05 | - | 4.29 14.80 1.05 | - 15.70 | <u>16.60</u> | - | 4.0 8.1 3.0 | 88 162 95 | 1690 8360 1920 | 568 1670 1390 | 2060 2320 823 | 5 5 3 | J-, | -266 -267 -268 | 1.0 m 1.0 m 1.0 m | 12.80 10.20 33.50 | | 12.80 10.20 35.50 | 33.50 | - 31.50 | - | 15.4 5.2 19.3 | 197 108 138 | 5640 3450 2180 | 540 347 592 | 3200 2270 5020 | 9 7 11 |
| J-103 0.5 m J-104 0.5 m | 0.20 | - | 0.20 | - | - | - | 4.2 | 138 121 | 5240 2010 | 885 204 | 453 406 | 2 X | J- | -269 -270 | 1.0 m 1.0 m | 79.30 94.75 | 47.90 116.00 | 79.30 96.40 | 94.75 | 93.10 | - | 49.2 34.7 | 450 1250 | 15900 5990 | 1870 1490 | 3410 9320 | 10 25 |
| J-105 0.5 m J-108 1.0 m | 1.58 0.27 | - | 1.58 0.27 | - | - | - | 1.9 X | 122 34 | 1280 389 | 392 13 | 440 376 | X X | | -273 -276 | 1.0 m 1.0 m | 0.16 0.14 | - | 0.16 0.14 | - | - | - | X 0.6 | 42 68 | 108 3690 | 17 97 | 35 283 | Х З |
| J-110 1.0 m J-111 1.0 m | 0.19 | - | 0.19 | - | - | - | X X | 40 74 | 172 399 | 11 46 | 144 44 | X X | J-, | -278 | 1.0 m 2.0 m | 1.83 195.00 | 202.00 | 1.83 195.00 | - | - | - | 6.7 39.1 | 404 1580 | 3810 16900 | 2190 9780 | 2130 22400 | 7 73 |
| J-113 1.0 m J-114 1.0 m J-116 1.0 m | 0.25 2.05 0.25 | - | 0.25 2.05 0.25 | - | - | - | 1.0 5.1 2.3 | 58 164 110 | 2520 258 2600 | 43 699 108 | 35 497 5 | X X X | J-, | -279 -280 -281 | 2.0 m 2.0 m 2.0 m | 4.32 0.64 0.97 | - | 4.32 0.64 0.97 | - | - - - | - | 3.6 8.3 9.1 | 318 279 161 | 5260 4920 7060 | 540 1150 139 | 1300 740 205 | 6 2 2 |
| J-110 1.0 m J-120 1.0 m J-121 1.0 m | 7.85 0.66 | - | 7.77 0.66 | - 7.85 - | - | - 7.93 - | 2.3 27.7 8.2 | 110 122 115 | 2360 805 | 108 110 104 | 3200 37 | 3 X | J- | -281 -282 -283 | 2.0 m 2.0 m 1.0 m | 0.97 18.90 0.11 | - | 18.90 0.11 | - | - | - | 22.1 X | 2530 53 | 15200 74 | 12700 28 | 203 2230 10 | 2 16 X |
| J-122 1.0 m J-123 1.0 m | 1.62 17.80 | - | 1.62 16.80 | - 17.80 | - 18.80 | - | 4.1 31.5 | 76 212 | 802 12600 | 84 186 | 2400 4030 | 4 6 | J- J- | -290 -291 | 1.0 m 1.0 m | 0.16 0.24 | - | 0.15 0.23 | 0.16 0.24 | 0.17 | - 0.24 | 2.7 4.1 | 46 87 | 720 2890 | 51 126 | 129 384 | X X |
| J-125 1.0 m J-131 1.0 m | 0.92 10.08 | - | 0.92 9.75 | - 10.08 | - 10.40 | - | 3.7 7.4 | 54 336 | 461 286 | 22 406 | 19 869 | X X | J- | -292 -299 | 1.0 m 2.0 m | 0.62 | - | 0.62 | - | - | - | 1.9 X | 65 51 | 3970 42 | 373 12 | 1070 49 | 7 X |
| J-132 1.0 m J-133 1.0 m J-134 1.0 m | 20.70 80.00 27.25 | 21.70 54.80 25.00 | 20.70 80.00 25.90 | 27.25 | - 28.60 | - | 1.6 10.5 4.1 | 167 759 363 | 454 2000 572 | 397 2390 1040 | 1570 5110 6590 | 4 8 9 | J- | -301 -302 -303 | 2.0 m 2.0 m 1.0 m | 0.23 0.24 30.60 | - 32.30 | 0.23 0.24 30.60 | - | | - | 4.9 1.2 14.4 | 136 114 2240 | 3750 3500 13100 | 25 122 10200 | 201 47 29000 | X X 60 |
| J-134 1.0 m J-135 1.0 m J-136 1.0 m | 23.75 88.85 | 18.50 86.50 | 23.50 23.50 83.90 | 23.75 | 28.00 24.00 93.80 | - | 5.2 38.1 | 277 253 | 316 2820 | 396 2410 | 3860 26800 | 13 41 | J- | -304 | 1.0 m 1.0 m | 25.55 79.35 | 32.50 74.40 | 23.90 68.40 | 25.55 | 27.20 90.30 | - | 23.4 58.9 | | | 17700 | | 136 143 |
| J-137 1.0 m J-138 1.0 m | 28.90 9.52 | 29.70 | 30.20 9.52 | | 27.60 | - | 10.5 37.3 | 85 105 | 759 373 | 516 437 | 18700 3000 | 32 8 | J- | | 1.0 m 1.0 m | 0.42 0.72 | - | 0.41 0.71 | 0.42 0.72 | - 0.73 | 0.42 - | 3.7 12.9 | 104 289 | 514 4660 | 89 177 | 14 28 | X 5 |
| J-143 1.0 m J-148 1.0 m | 0.19 | - | 0.19 | - | - | - | X 0.5 | 22 47 | 85 118 | 18 45 | 20 98 | X X | J- | -318 | 2.0 m 2.0 m | 0.22 | - | 0.22 | - | - | - | 0.7 | 63 66 | 147 147 | 41 37 | 134 12 | 2 X |
| J-156 1.0 m J-161 1.0 m | 0.13 5.10 108.50 | - - 129.00 | 0.13 5.10 101.00 | - - 108.50 | - 116.00 | - | X 1.8 40.8 | 18 68 306 | 125 752 1860 | 8 223 1250 | 27 1050 16200 | X 3 23 | J-, | | 2.0 m 2.0 m 2.0 m | 0.44 0.47 0.62 | - | 0.44 0.47 0.62 | - | | - | 0.7 X 3.0 | 83 43 72 | 260 45 6480 | 209 19 366 | 15 12 33 | X X 3 |
| J-162 1.0 m J-163 1.0 m J-164 1.0 m | 108.50 15.45 4.17 | 129.00 19.90 | 101.00 16.60 4.17 | | 116.00 14.30 - | | 40.8 7.7 1.2 | 236 50 | 1860 1470 724 | 540 | 4040 757 | 8 | J- | -329 | 2.0 m 2.0 m 2.0 m | 0.62 | - | 0.62 | 0.21 | 0.21 | 0.21 | 3.0 12.9 14.1 | 94 | 2790 13400 | 943 | 33 41 10 | X X |
| J-165 1.0 m J-166 0.5 m | 27.00 4.74 | <u>15.00</u> | 27.00 4.74 | | - | - | 18.0 3.3 | 411 114 | 1140 1660 | 577 | 4870 881 | 9 2 | J- | -333 | 1.0 m 2.0 m | 0.67 | - | 0.67 | - | - | - | 9.9 16.0 | 291 383 | 9610 13000 | 838 | 16 539 | X X X |
| J-167 0.5 m J-168 0.5 m | 29.00 10.20 | 34.20 - | 27.60 10.40 | 10.20 | 30.40 10.00 | - | 6.3 4.6 | 113 121 | 1800 2820 | 504 882 | 4340 2670 | 8 4 | J-, J-, | -335 -336 | 2.0 m 2.0 m | 2.86 0.16 | - | 2.86 0.16 | - | - | - | 11.8 X | 132 31 | 5950 198 | 375 45 | 1540 99 | 9 X |
| J-169 0.5 m J-170 0.5 m | 16.00 22.30 | - 15.40 | 16.00 22.30 | - | - | - | 6.9 6.1 | 149 153 | 1910 2240 | 445 | 3100 6560 | 4 | J- | -338 | 2.0 m | 0.10 | - | 0.10 | - | - | - | Х | 29 | 171 | 60 | 40 | Х |
| J-171 0.5 m J-172 0.5 m | 3.93 44.10 21 25 | 36.10 26.00 | 3.93 44.10 21.90 | | | - | 2.0 64.5 | | 1440 23800 8240 | | 917 8890 5460 | 3 19 11 | | | | | | | | | | | | | | | |
| J-173 0.5 m J-174 0.5 m J-175 0.5 m | 21.25 27.95 38.15 | 26.00 23.60 38.40 | 21.90 29.10 40.70 | 27.95 | 20.60 26.80 35.60 | - | 19.6 9.5 7.0 | 337 197 118 | 8240 4340 2590 | 1820 | 5460 6470 29400 | 11 10 39 | | | | | | | | | | | | | | | |
| J-175 0.5 m J-176 1.0 m J-177 1.0 m | 74.20 0.25 | 59.90 | 62.80 0.24 | | 85.60 | - 0.25 | 17.0 0.6 | 77 | 1810 190 | | 4400 61 | 8 X | | | | | | | | | | | | | | | |
| J-178 1.0 m J-181 1.0 m | 0.65 1.00 | - | 0.65 | - | - | - | X 0.5 | 35 30 | 131 110 | 12 6 | 268 20 | X X | | | | | | | | | | | | | | | |
| J-183 1.0 m | 0.13 | - | 0.13 | - | - | - | Х | 33 | 104 | 7 | 51 | Х | | | | | | | | | | | | | | | |

The following information is provided to comply with the JORC Code (2012) requirements for the reporting of the previous exploration and drilling results for Exploration Licence 1595 in Papua New Guinea.

| | | JORC | CODE 2012 |
|--------------------------|---|--|--|
| | | Section 1 Sampli | ng Techniques and Data |
| Criteria | | Explanation | Commentary |
| Sampling techniques | 0 | Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. | Samples locations were surveyed (averaged) utilising a handheld GPS, with reference to topographic maps etc. Logging of outcrop and grab rock samples normally included mineralisation, lithology, weathering, alteration, structure, texture. Sampling protocols and QAQC are as per industry best practice procedures. |
| | 0 | Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. | Standard industry practice sampling procedures were followed. |
| | 0 | Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1m samples from which 3 kg was pulverised to produce a 30g charge for fire assay') In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information. | Swit Kia channel samples were collected in multiple metre, single metre and parts of metres relative to the intensity of mineralisation and alteration exhibited. They were driven to Lae for sample preparation in Papua New Guinea by Laboratory SGS Australia Pty Ltd and analysis in Townsville by fire assay (50g charge) for gold and ICP for copper, molybdenum, silver, lead, zinc, arsenic, antimony and other elements. Gravimetric gold analysis was subsequently undertaken for samples with high concentrations of arsenic, that may have (but didn't apparently) interfered with the process. Samples were collected in calico bags for despatch to the laboratory. Sample preparation was in 3-5kg pulverising mills, followed by splitting to a 140g pulp which was analysed by 50 gram Fire Assay and Inductively Coupled Plasma Optical (Atomic) Emission Spectrometry Multi-acid digest including Hydrofluoric, Nitric, Perchloric and Hydrochloric acids. |
| Drilling techniques | 0 | Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). | No drilling. |
| Drill sample recovery | 0 | Method of recording and assessing core and chip sample recoveries and results assessed | No drilling. |
| | 0 | Measures taken to maximise sample recovery and ensure representative nature of the samples. | No drilling. |
| | 0 | Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. | No drilling. |
| Logging | 0 | Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. | No drilling. |

| | 0 | Whether logging is qualitative or | No drilling. |
|---|--------|---|--|
| | | quantitative in nature. Core (or costean, | |
| | 0 | channel, etc) photography. The total length and percentage of the | No drilling. |
| | | relevant intersections logged | |
| Sub-sampling techniques and sample | 0 | If core, whether cut or sawn and whether quarter, half or all core taken. | No drilling. |
| preparation | 0 | If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. | No drilling. |
| | 0 | For all sample types, the nature, quality and appropriateness of the sample preparation technique. | No drilling. |
| | 0 | Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. | No drilling. |
| | 0 | Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate /second-half sampling. | No drilling. |
| | 0 | Whether sample sizes are appropriate to the grain size of the material being sampled. | No drilling. |
| Quality of assay data and laboratory tests | 0 | The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. | Assaying techniques utilised can be considered to be appropriate. For the ICP analyses, the technique is considered to be 'total'. |
| | o | Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established. | Acceptable levels of accuracy and precision have been established with duplicate and repeat analyses. Gravimetric analysis was undertaken for samples with high concentrations of arsenic, that may have interfered with the process (but didn't apparently). |
| | 0 | For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. | No such tools |
| Verification of sampling and assaying | 0 | The verification of significant intersections by either independent or alternative company personnel. | Verified by P.McNeil and mapped / verified by Consultant Geologist Ken Igara. |
| | 0 | The use of twinned holes. | No holes have been twinned |
| | 0 | Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. | Primary data was collected manually then loaded into the database. |
| | 0 | Discuss any adjustments to assay data. | No adjustments or calibrations have been made to any assay data. |
| Location of data points | 0 | Accuracy + quality of surveys used to locate drill holes (collar + down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. | Not applicable. A hand held GPS (averaged) was used to determine collar locations. |
| | 0 0 | Specification of the grid system used. Quality and adequacy of topographic control. | Map datum is AGD 066. 40m contours from 1:100,000 plans, 10m from SRTM contours. |
| Data spacing and | 0 | Data spacing for reporting of Exploration Results. | Refer to the attached plans for data spacing of exploration results. |
| distribution | 0 | Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied | The data spacing and distribution is insufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation |

| | 0 | Whether sample compositing has been applied. | No sample compositing has been applied. |
|---|---|--|---|
| Orientation of data in relation to geological structure | 0 | Whether the orientation of sampling achieves unbiased sampling of possible structures to the extent this is known, considering the deposit type. | The orientation of sampling achieves unbiased sampling of possible structures to the extent to which this is known, considering the deposit type and outcrop available to sample. |
| Structure | 0 | If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported. | The relationship between the drilling orientation and the orientation of key mineralised structures is NOT considered to have introduced any sampling bias, but has constrained the possible mineralised region. |
| Sample security | 0 | The measures taken to ensure sample security | Samples were retained by Company personnel until they were despatched at the Lae laboratory. There are no issues with sample security. |
| Audits or reviews | 0 | The results of any audits or reviews of sampling techniques and data. | No specific audits or reviews of sampling techniques and data have been undertaken. |

| | Section 2 Reporting of Exploration Results | | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--|--|--|
| Criteria | | Explanation | Commentary | | | | | | | | |
| Mineral tenement and land tenure status | 0 | Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. | Exploration Licence 1595 - Bulago is located in Papua New Guinea's Hella Province. There no agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental issues associated with the EL. | | | | | | | | |
| | 0 | The security of the tenure held at the time of | The PNG National government under the Mining Act of 1992 currently has the right to acquire up to 30% of any project at the time of granting of a mining lease for the 'sunk cost'. The tenement is in good standing and FNT will seek renewal in | | | | | | | | |
| | 0 | reporting along with any known impediments to obtaining a licence to operate in the area. | July 2014. No known impediments exist apart from the geographic isolation and the necessity for creating and maintaining good relationships with local landowners. | | | | | | | | |
| Exploration done by other parties | 0 | Acknowledgment and appraisal of exploration by other parties. | Exploration in the region was initiated in the late 1960s as part of a PNG porphyry copper deposit search. It was explored for gold initially in the early 1980's, with little work since 1987 and prior to FNT. | | | | | | | | |
| Geology | 0 | Deposit type, geological setting and style of mineralisation. | High grade intrusive -epithermal related gold and porphyry copper-gold - molybdenum targets. | | | | | | | | |
| Drill hole information | 0 | A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: | No drilling. | | | | | | | | |
| | | Easting and northing of the drill hole collar | No drilling. | | | | | | | | |
| | | Elevation or RL (Reduced Level- elevation above sea level in metres) of the drill hole collar | No drilling. | | | | | | | | |
| | | Dip and azimuth of the hole | No drilling. | | | | | | | | |
| | | Down hole length and interception depth | No drilling. | | | | | | | | |
| | | Hole length | No drilling. | | | | | | | | |
| | 0 | If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. | No drilling. | | | | | | | | |

Section 2 -- Reporting of Exploration Results

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| Data aggregation methods | 0 | In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. | Tables of results included show data aggregation if applied in trench/channel samples etc. No top cuts have been applied. They are continuous samples and so are stated as continuous weighted assay results (length x grade summed for each sample / sum of total length). |
|---|---|--|---|
| | | Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail | Is this occurs, it is stated in the text. |
| | 0 | The assumptions used for any reporting of metal equivalent values should be clearly stated. | No metal equivalent values are reported. |
| Relationship between mineralisation | 0 | These relationships are particularly important in the reporting of Exploration Results. | Well understood |
| widths & intercept lengths | 0 | If the geometry of the mineralisation with respect to drill hole angle is known, its nature should be reported. | The 'down outcrop or downhole sampled lengths have been reported because the geometry of the mineralisation with respect to the sampling orientation has not been properly constrained. |
| | 0 | If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known'). | |
| Diagrams | 0 | Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views. | Appropriate maps, sections and tabulations of intercepts are included. |
| Balanced reporting | 0 | Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results. | Comprehensive reporting of Exploration Results has been previously released. |
| Other substantive exploration data | 0 | Other exploration data, if meaningful and material should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances | All meaningful exploration data has been included. |
| Further work | 0 | The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). | Drilling is dependent on subsequent capital raising. |
| | 0 | Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive. | Appropriate plans will be included, as possible in a later release documenting future work. |

| | Frontier Resources Ltd Exploration Licence Information | | | | | | | | | | | |
|---------------------|--|--------------|--------------|---|------------------------------|---------------------------|----------------------------|-------------------------|--|--|--|--|
| | Licence No. | Date From | Date To | Ownership | 'Reduced' Area (SQ KM) | Latitudinal Sub Blocks | Current Area (SQ KM) | Latitudina Sub Block | | | | |
| Bulago River | EL 1595 | 7/07/2012 | 6/7/2014 | 100% Frontier Gold PNG Ltd | 100 | 30 | 140 | 42 | | | | |
| Mt Andewa | EL 1345 | 13/08/2012 | 12/8/2014 | 100% Frontier Copper PNG Ltd | 100 | 30 | 117 | 35 | | | | |
| Mt Likuruanga | EL 1351 | 13/08/2012 | 12/8/2014 | 100% Frontier Copper PNG Ltd | 100 | 30 | 123 | 37 | | | | |
| East New Britain | EL 1592 | 21/03/2013 | 20/3/2015 | 100% Frontier Copper PNG Ltd | 100 | 30 | 493 | 148 | | | | |
| Central New Britain | EL 1598 | 21/03/2013 | 20/3/2015 | 100% Frontier Copper PNG Ltd | 100 | 30 | 347 | 104 | | | | |
| Leonard Schultz | EL 1597 | 13/02/2013 | 12/2/2015 | 10% Deferred Carried to BFS Frontier Gold PNG Ltd - FrontRunner Exploration Ltd JV | To be relinquished | 47 | 590 | 177 | | | | |
| Cethana | EL 29/2009 | 13/09/2010 | 12/09/2015 | 10% Free Carried to BFS Frontier -Torque Mining Ltd JV | 109 | | 109 | NA | | | | |
| River Lea | EL 42/2010 | 3/04/2011 | 2/04/2016 | 10% Free Carried to BFS Frontier -Torque Mining Ltd JV | 9 | | 9 | NA | | | | |
| Narrawa Creek | RL 3/2005 | 12/05/2006 | 12/05/2014 | 10% Free Carried to BFS Frontier -Torque Mining Ltd JV | 2.8 | | 2.8 | NA | | | | |
| Stormont Mine | ML 1/2013 | 3/11/2013 | 13/08/2018 | 5% Nett Profits Interest Frontier -Torque/BCD Mining Ltd JV | 0.13 | | 0.13 | NA | | | | |
| | | Total Reduce | d PNG Area = | 500 SQ KM | 621 | SQ KM | 1,931 | SQ KM | | | | |

2. The PNG Government maintains the right to purchase up to 30% project equity at "Sunk Cost" if/when a Mining Lease is granted.

3. BFS = Completion of a positive and hence "Bankable" Feasibility Study into the viability of any proposed mining operation