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ASX Announcement

Isabel Nickel Project Phase 2 drilling update

Highlights

- Phase 2 of resource definition drilling continues, with encouraging results including 12.0m @ 1.34% Ni from surface including 5.0m @ 1.82% Ni from 3.0m.
- Additional results highlighting both high grade limonite and saprolite intersections include:
 - 14.2m @ 1.73% Ni from surface including 2.0m @ 1.65% Ni from 4.0m (limonite) and 7.5m @ 2.17% Ni from 6.0m (saprolite)
 - 11.0m @ 1.74% Ni from surface including 2.5m @ 2.05% Ni from 3.0m (limonite) and 4.7m @ 2.35% Ni from 5.5m (saprolite)
 - 9.8m @ 1.61% Ni from 1.0m including 3.0m @ 1.22% Ni from 1.0m (limonite) and 5.0m @ 2.09% Ni from 4.0m (saprolite)
 - 14.0m @ 1.49% Ni from 4.0m including 5.0m @ 1.64% Ni from 6.0 (limonite) and 4.4m @ 2.04% Ni from 11.0m (saprolite)
 - 14.0m @ 1.49% Ni from 2.0m including 3.0m @ 1.87% Ni from 6.0 (limonite) and 6.0m @ 1.96% Ni from 9.0m (saprolite)
- Upgrade of JORC Resource estimate on track for announcement next month.

Axiom Mining Limited ('Axiom') is pleased to announce further drilling results from Phase 2 of its resource definition drilling program on the Isabel Nickel Project in Solomon Islands.

The latest results further affirm the presence of high grade laterite in other areas within the tenement.

These drilling results will upgrade Axiom's Maiden JORC Resource Estimate initially released on 30 September 2015.

Continues on page 2



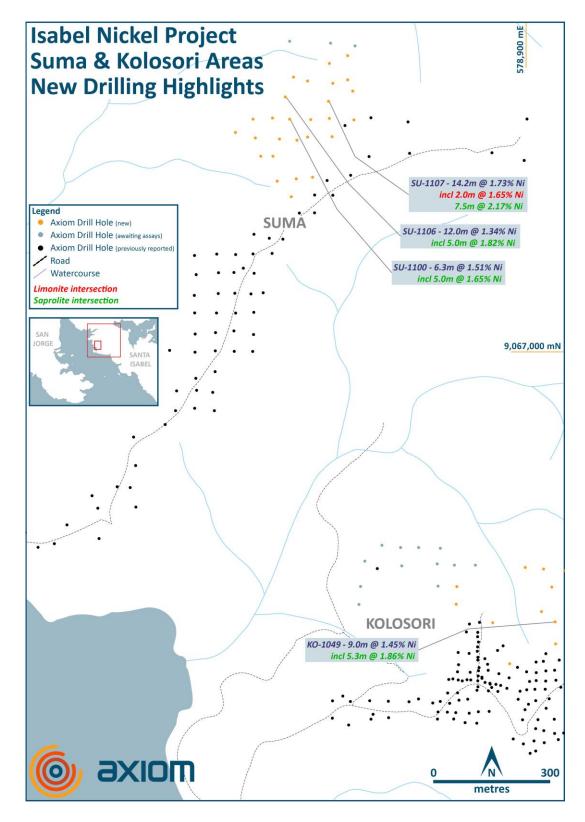


Figure 1 New drilling highlights at Kolosori and Suma prospect areas



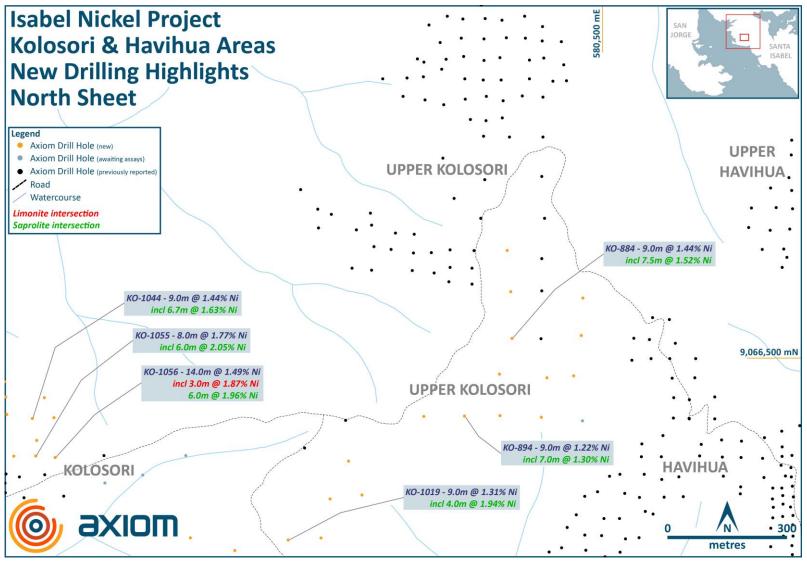


Figure 2 New drilling highlights at Kolosori and Havihua prospect areas



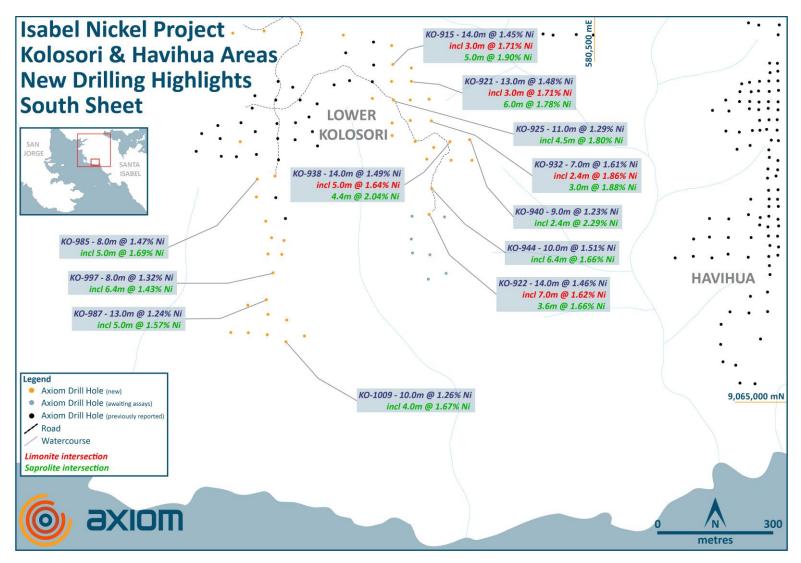


Figure 3 New drilling highlights at Kolosori and Havihua prospect areas



Exploration Results

Table 1 Results for new drill holes for Kolosori and Suma prospect areas (NB: Holes may be reported out of sequential order; missing holes will be reported as assays are available)

Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
KO-1000	8.5m @ 0.98% Ni from 1.5m			579654.8	9065227	231.0	12.0
KO-1001	4.0m @ 1.33% Ni from surface		1.4m @ 1.89% Ni from 1.6m	579703.7	9065212	198.5	12.0
KO-1003	10.0m @ 1.16% Ni from surface		4.0m @ 1.51% Ni from 3.0m	579558.7	9065180	185.6	14.6
KO-1004	8.0m @ 1.14% Ni from 1.0m	2.0m @ 1.25% Ni from 2.0m	2.0m @ 1.58% Ni from 4.0m	579604.0	9065179	183.2	9.0
KO-1005	1.5m @ 1.00% Ni from surface			579653.0	9065174	174.0	10.0
KO-1009	10.0m @ 1.26% Ni from 1.0m		4.0m @ 1.67% Ni from 6.0m	579701.2	9065156	172.2	13.5
KO-1010	3.4m @ 1.36% Ni from surface		2.5m @ 1.55% Ni from 0.5m	579749.3	9065171	180.6	10.8
KO-1017	3.7m @ 0.85% Ni from surface			580451.0	9066650	361.0	6.0
KO-1019	9.0m @ 1.31% Ni from 3.0m		4.0m @ 1.94% Ni from 7.0m	579712.0	9066043	349.0	14.4
KO-1020	8.0m @ 1.28% Ni from 5.0m	2.0m @ 1.67% Ni from 8.0m	2.0m @ 1.66% Ni from 10.0m	579794.0	9066048	359.0	15.6
KO-1035	1.0m @ 0.81% Ni from surface			578899.0	9066448	113.0	5.0
KO-1036	1.0m @ 0.76% Ni from surface			578946.0	9066444	134.0	5.0
KO-1037				579000.0	9066440	148.0	6.0
KO-1038	1.0m @ 0.86% Ni from surface			578967.1	9066398	124.1	5.0
KO-1039	1.0m @ 1.95% Ni from 1.0m		1.0m @ 1.95% Ni from 1.0m	579003.0	9066402	165.0	5.0
KO-1040	7.7m @ 1.09% Ni from 1.0m		2.0m @ 1.48% Ni from 4.0m	579100.0	9066400	188.0	12.0
KO-1042	3.0m @ 1.14% Ni from surface	2.0m @ 1.28% Ni from surface		578940.6	9066335	125.9	7.0
KO-1043	3.0m @ 1.13% Ni from surface		1.0m @ 1.55% Ni from 1.0m	579006.0	9066358	158.0	7.0
KO-1044	9.0m @ 1.44% Ni from surface		6.7m @ 1.63% Ni from 0.3m	579070.0	9066348	184.0	10.5



Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
KO-1045	3.2m @ 0.85% Ni from 1.0m			579124.0	9066350	184.0	8.0
KO-1046				578815.4	9066306	112.0	5.0
KO-1049	9.0m @ 1.45% Ni from surface		5.3m @ 1.86% Ni from 1.7m	578975.6	9066308	143.7	12.0
KO-1050	5.0m @ 0.83% Ni from 1.0m			579081.0	9066293	204.0	10.0
KO-1053	4.0m @ 1.27% Ni from surface			578976.9	9066252	154.5	12.0
KO-1054	10.8m @ 1.02% Ni from 1.2m		1.5m @ 1.57% Ni from 1.5m	579023.4	9066253	172.4	16.0
KO-1055	8.0m @ 1.77% Ni from surface		6.0m @ 2.05% Ni from surface	579078.6	9066254	188.4	11.0
KO-1056	14.0m @ 1.49% Ni from 2.0m	3.0m @ 1.87% Ni from 6.0m	6.0m @ 1.96% Ni from 9.0m	579127.0	9066250	211.0	17.5
KO-1057	2.0m @ 1.57% Ni from surface		1.3m @ 1.74% Ni from 0.7m	578859.0	9066201	162.0	6.0
KO-1077	10.0m @ 1.29% Ni from surface	2.0m @ 1.75% Ni from 2.0m	3.2m @ 1.42% Ni from 4.0m	578723.2	9066399	102.2	14.0
KO-880	3.0m @ 0.77% Ni from surface			580128.0	9066900	271.0	7.0
KO-882	5.0m @ 0.93% Ni from 1.0m			580261.1	9066769	314.5	11.0
KO-883	3.0m @ 0.99% Ni from surface		1.0m @ 1.34% Ni from 1.0m	580270.2	9066666	320.9	8.0
KO-884	9.0m @ 1.44% Ni from surface		7.5m @ 1.52% Ni from 0.5m	580273.2	9066549	346.6	11.0
KO-886	3.7m @ 0.86% Ni from 3.0m			580447.0	9066556	373.0	9.2
KO-889				580241.7	9066459	367.4	5.0
KO-890	5.5m @ 1.09% Ni from surface			580361.0	9066450	438.0	7.0
KO-891	5.0m @ 1.22% Ni from 1.0m		3.0m @ 1.52% Ni from 3.0m	580428.0	9066455	342.0	8.3
KO-893	4.5m @ 0.90% Ni from 1.0m			580052.0	9066353	344.0	11.3
KO-894	9.0m @ 1.22% Ni from 1.0m		7.0m @ 1.3% Ni from 2.0m	580154.0	9066354	368.0	10.4
KO-895	14.0m @ 0.88% Ni from 1.0m			580243.0	9066355	347.0	17.7



Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
KO-896	7.0m @ 1.13% Ni from surface		4.0m @ 1.37% Ni from 1.0m	580347.0	9066351	322.0	10.4
KO-898	13.0m @ 0.93% Ni from 3.0m			579863.0	9066241	349.0	17.8
KO-900	4.5m @ 0.93% Ni from 1.0m			579817.0	9066146	346.0	8.0
KO-901	3.0m @ 0.84% Ni from 1.0m			579897.0	9066156	335.0	7.2
KO-903				579466.3	9066049	280.8	4.0
KO-904	5.0m @ 0.99% Ni from 2.0m		2.0m @ 1.46% Ni from 5.0m	579577.9	9066017	306.1	11.8
KO-907	5.5m @ 0.70% Ni from 2.0m			579563.7	9065955	300.3	9.7
KO-908	3.2m @ 0.84% Ni from 2.0m			579644.6	9065961	312.5	8.6
KO-909	13.0m @ 0.98% Ni from 2.0m		3.5m @ 1.27% Ni from 7.5m	579742.4	9065957	355.7	19.2
KO-910	1.0m @ 0.61% Ni from 2.0m			579850.0	9065950	0.0	9.0
KO-912	5.0m @ 1.34% Ni from 1.0m		2.0m @ 1.76% Ni from 2.0m	579975.0	9065923	295.0	8.0
KO-915	14.0m @ 1.45% Ni from 1.0m	3.0m @ 1.71% Ni from 5.0m	5.0m @ 1.90% Ni from 8.0m	579978.0	9065874	303.0	16.5
KO-916	4.0m @ 1.12% Ni from surface			580026.0	9065865	305.0	8.0
KO-920	8.4m @ 1.16% Ni from 4.0m	3.0m @ 1.43% Ni from 7.0m	1.0m @ 1.38% Ni from 10.0m	579974.8	9065830	315.4	15.0
KO-921	13.0m @ 1.48% Ni from 2.0m	3.0m @ 1.71% Ni from 6.0m	6.0m @ 1.78% Ni from 9.0m	580026.0	9065830	316.8	15.0
KO-922	14.0m @ 1.46% Ni from 1.0m	7.0m @ 1.62% Ni from 3.0m	3.6m @ 1.66% Ni from 10.0m	580072.0	9065486	213.8	15.0
KO-924	2.0m @ 0.85% Ni from surface			579925.0	9065786	328.0	5.5
KO-925	11.0m @ 1.29% Ni from 1.0m		4.5m @ 1.8% Ni from 6.5m	579979.9	9065782	311.3	14.3
KO-926	4.5m @ 0.86% Ni from 1.0m			580029.0	9066777	308.0	8.0
KO-927	12.0m @ 1.11% Ni from 2.0m		4.0m @ 1.34% Ni from 10.0m	580072.0	9065784	294.0	16.0
KO-930	2.0m @ 0.73% Ni from surface			579976.2	9065722	298.9	7.0



Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
KO-931	4.0m @ 1.02% Ni from surface		1.0m @ 1.46% Ni from 1.0m	580023.5	9065729	287.7	8.0
KO-932	7.0m @ 1.61% Ni from 7.0m	2.4m @ 1.86% Ni from 8.6m	3.0m @ 1.88% Ni from 11.0m	580078.0	9065728	284.0	17.0
KO-935	1.0m @ 0.74% Ni from 1.0m			579976.2	9065690	294.3	5.0
KO-936	8.0m @ 1.10% Ni from 2.0m		2.0m @ 1.38% Ni from 6.0m	580036.0	9065675	271.3	12.0
KO-937	2.3m @ 0.99% Ni from 0.7m			580084.0	9065659	264.0	10.0
KO-938	14.0m @ 1.49% Ni from 4.0m	5.0m @ 1.64% Ni from 6.0m	4.4m @ 2.04% Ni from 11.0m	580126.0	9065674	268.0	18.0
KO-940	9.0m @ 1.23% Ni from surface		2.4m @ 2.29% Ni from 5.6m	580177.1	9065679	249.3	10.5
KO-941	4.0m @ 0.91% Ni from surface		1.0m @ 1.28% Ni from 1.0m	580066.0	9065629	253.0	7.5
KO-942	4.0m @ 1.12% Ni from 2.0m		2.0m @ 1.34% Ni from 3.0m	580129.0	9065626	249.0	8.0
KO-943	6.0m @ 0.85% Ni from 3.0m			580186.7	9065631	236.3	12.0
KO-944	10.0m @ 1.51% Ni from surface		6.4m @ 1.66% Ni from 3.0m	580079.0	9065552	242.0	11.0
KO-976	7.0m @ 1.06% Ni from surface		1.0m @ 1.81% Ni from 2.0m	579583.0	9065674	316.0	14.6
KO-985	8.0m @ 1.47% Ni from 1.0m		5.0m @ 1.69% Ni from 3.0m	579627.0	9065577	309.0	10.0
KO-987	13.0m @ 1.24% Ni from 1.0m		5.0m @ 1.57% Ni from 4.0m	579650.6	9065265	246.4	17.2
KO-988	6.3m @ 1.27% Ni from 1.0m		3.3m @ 1.63% Ni from 4.0m	579625.0	9065531	296.0	9.5
KO-990	3.0m @ 1.77% Ni from surface		2.0m @ 2.17% Ni from 1.0m	579602.8	9065251	232.0	9.5
KO-991	13.0m @ 1.00% Ni from surface		3.0m @ 1.46% Ni from 8.0m	579649.0	9065468	277.0	13.0
KO-993	13.0m @ 1.34% Ni from 1.0m	3.0m @ 1.80% Ni from 4.0m	3.0m @ 1.60% Ni from 7.0m	579664.0	9065425	264.0	14.0
KO-994	8.0m @ 1.31% Ni from surface		4.0m @ 1.58% Ni from 3.0m	579696.0	9065418	259.0	12.0
KO-995	3.0m @ 0.97% Ni from 2.0m		1.0m @ 1.49% Ni from 3.0m	579654.8	9065383	244.2	9.0
KO-996	4.0m @ 1.03% Ni from surface		1.0m @ 1.28% Ni from 2.0m	579690.5	9065382	310.4	8.5



Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
KO-997	8.0m @ 1.32% Ni from 1.0m		6.4m @ 1.43% Ni from 1.6m	579667.8	9065334	303.9	11.4
SU-1085	2.5m @ 1.07% Ni from surface			578298.0	9067399	122.0	6.0
SU-1086	6.0m @ 1.03% Ni from surface			578262.0	9067439	103.0	10.5
SU-1087	2.0m @ 0.77% Ni from surface			578310.9	9067454	121.7	4.0
SU-1088	4.4m @ 1.24% Ni from surface	3.4m @ 1.32% Ni from 1.0m		578351.8	9067454	134.9	7.0
SU-1089	3.0m @ 0.72% Ni from surface			578251.0	9067503	95.0	10.0
SU-1090	2.0m @ 0.84% Ni from surface			578220.0	9067503	97.0	10.5
SU-1091	1.0m @ 0.80% Ni from surface			578155.0	9067564	104.0	10.0
SU-1092	1.0m @ 0.79% Ni from surface			578206.0	9067550	113.0	7.0
SU-1093				578268.0	9067547	121.0	5.0
SU-1094	1.6m @ 0.83% Ni from surface			578313.0	9067544	137.0	7.0
SU-1095	2.5m @ 0.94% Ni from surface			578340.0	9067552	147.0	11.3
SU-1096				578401.7	9067556	151.8	7.0
SU-1098				578200.0	9067598	110.0	8.0
SU-1099	6.0m @ 1.13% Ni from 1.0m		2.0m @ 1.48% Ni from 3.0m	578250.0	9067601	136.0	9.0
SU-1100	6.3m @ 1.51% Ni from 1.0m		5.0m @ 1.65% Ni from 2.0m	578294.0	9067598	139.0	11.0
SU-1101	6.0m @ 0.80% Ni from surface			578348.0	9067597	136.0	11.0
SU-1102	1.7m @ 1.00% Ni from surface			578396.0	9067600	158.0	12.0
SU-1103				578459.0	9067596	168.0	9.2
SU-1106	12.0m @ 1.34% Ni from surface		5.0m @ 1.82% Ni from 3.0m	578283.0	9067655	122.0	14.3
SU-1107	14.2m @ 1.73% Ni from surface	2.0m @ 1.65% Ni from 4.0m	7.5m @ 2.17% Ni from 6.0m	578394.0	9067644	160.0	15.9



Hole ID	Entire intersection	Limonite intersection	Saprolite intersection	Easting	Northing	RL (m)	EOH (m)
SU-1108	13.2m @ 1.24% Ni from 3.0m	6.0m @ 1.33% Ni from 6.0m	2.0m @ 1.55% Ni from 12.0m	578456.0	9067670	167.0	18.0
SU-1113	3.0m @ 1.37% Ni from surface		2.0m @ 1.56% Ni from surface	578304.0	9067706	111.0	14.8
SU-1114	8.0m @ 1.02% Ni from surface		1.5m @ 1.35% Ni from 1.0m	578340.0	9067696	125.0	8.0
SU-1115	2.0m @ 0.72% Ni from surface			578405.0	9067690	135.0	9.0
SU-1116	4.5m @ 1.3% Ni from surface		1.8m @ 1.74% Ni from 2.7m	578443.0	9067699	160.0	9.0
SU-1123	8.0m @ 1.11% Ni from 1.0m		3.4m @ 1.42% Ni from 3.6m	578396.0	9067741	137.0	14.3
SU-1124	6.0m @ 0.97% Ni from surface			578443.0	9067761	144.0	11.0
SU-1129	2.3m @ 0.94% Ni from 1.2m		1.0m @ 1.33% Ni from 1.2m	578294.0	9067798	100.0	10.0
SU-1130	9.8m @ 1.61% Ni from 1.0m	3.0m @ 1.22% Ni from 1.0m	5.0m @ 2.09% Ni from 4.0m	578354.0	9067803	108.0	10.8
SU-1131	11.0m @ 1.74% Ni from surface	2.5m @ 2.05% Ni from 3.0m	4.7m @ 2.35% Ni from 5.5m	578399.0	9067793	118.0	13.0
SU-1132	5.8m @ 0.96% Ni from surface			578462.0	9067786	146.0	8.0
SU-1133	4.0m @ 1.65% Ni from surface		2.0m @ 2.13% Ni from 1.6m	578402.0	9067843	112.0	7.0

Notes to Table 1

0.6% Ni cut-off for entire intersection 1.2% Ni cut-off and >2.0m thickness for limonite intersection 1.2% Ni cut-off and >1.0m thickness for saprolite intersection Zone WGS84 UTM 57S, subject to final survey



Section 1: Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representation and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1.0m samples from which 3kg was pulverised to produce a 30g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	Currently utilising NQ single tube core in sampled intervals. Handheld XRF analysers were used infield for initial analysis to guide site geologist or field assistants in deciding to end the hole. Samples were collected generally at 1.0m interval. In changes in geology a range of intervals from 0.3m minimum to 1.25m maximum. Whole core samples were sent to the laboratory.
Drilling techniques	Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	NQ single tube by tungsten carbide bit employing man portable machines commonly used in laterite drilling in Indonesia and the Philippines. Holes were drilled vertically through the limonite and saprolite zones into underlying basement.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	NQ coring was by single tube to maximise core recovery. Average sample recovery exceeded 97%. In most cases laterite core recoveries exceeded 100% due to "swelling"—bit cuttings getting into the inner tube. Axiom has implemented a dry drilling technique in the top limonite zone and a low water technique in lower saprolite zone—bringing average recoveries on the laterite profile to more than 99%. Un-mineralised bedrock core recovery is below 90% average.



Criteria	JORC Code explanation	Commentary
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged.	 All holes were: marked up for recovery calculations geologically marked up and logged marked up for sampling interval and density determination photographed. In-situ wet density is determined by calliper method for limonite and saprolite and water displacement method for irregular shaped rocky saprolite and bed rock. A 10cm length of representative limonite and saprolite sample is selected for density measurement. For irregular rock sample, 5cm to 8cm core representing the lithology is sampled for density. Core was also geotechnically logged for hardness, fractures, fracture frequency, recovery and mining characteristics. All laterite intersections were analysed by standard laboratory techniques for mine grade and trace element values using fused bead XRF method.
Sub- sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all subsampling stages to maximise representation of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/secondhalf sampling. Whether sample sizes are appropriate to the grain size of the material being sampled.	Whole core was delivered to the laboratory. All sample reduction protocols were by standard laboratory techniques. A range of OREAS nickel laterite standards were inserted into the suite of samples. Blank samples were also inserted. These were inserted 1–2 in every batch of samples (150–200 samples) for all drilling samples submitted. Core duplicates are collected by splitting the previous sample interval. Duplicates are collected one in every 20 holes (5%) drilled. Laboratory standards and blanks were inserted into every 20 samples submitted plus repeats were completed every 50 samples.



Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	 Standard laboratory techniques as outlined below were undertaken: All samples were weighed wet, dried at 90 degrees and then weighed dry to establish minimum moisture ranges and density guides. Further drying to 105 degrees prior to reduction to remove all moisture. Standard reduction techniques were: jaw crusher pulveriser split to reduce sample to 200g. Ore grade by XRF fusion method. Loss on Ignition (LOI) by thermo gravimetric analysis. Where required, trace element analysis for selected elements or 30 element suite completed by four acid digest and AAS readings.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data.	Eight core holes twinned existing INCO or Kaiser pits or INCO GEMCO drill holes during the early part of the drilling program. One Axiom hole was twinned by an additional NQ triple tube core hole 100cm offset. One Axiom hole twinned by an additional HQ hole at 80 degrees. Six Axiom holes were recently twinned samples of which will be used for metallurgical test work.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control.	Initial collar location was by handheld GPS reading to 5.0m accuracy. After completing the hole, collars are again picked up by GPS for actual location. All collars are picked up by surveyors using differential Trimble DGPS.
Data spacing and distribution	Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied.	The current release covers drilling on 50.0m x 50.0m hole spacing. And in few instances on 100m x 100m spacing. The expected outcome of the 50m x 50m and the 100m x 100m hole spacing are appropriate for indicated and inferred resource categories, respectively.



Criteria	JORC Code explanation	Commentary
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The nickel laterite is a weathered geomorphic surface drape over ultramafic source units. All holes and pits were vertical and will be 100% true intersection.
Sample security	The measures taken to ensure sample security.	All samples were escorted offsite to a secure facility at the site camp. On-site security was provided for samples. Samples were bagged in polyweave bags and zip tied. Chain of custody protocols in place for transport from laboratories.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	Axiom has employed highly experienced nickel laterite consultants to review all procedures and results from the 2014 and 2015 drilling phases. This includes, drill types, depths, collar patterns, assay and other statistical methods.

Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	Prospecting Licence 74/11—80% held by Axiom. 50-year land lease—80% owned by Axiom. The validity of both the Prospecting Licence and the leasehold was tested and confirmed in a recent Solomon Islands High Court judgment. The hearing for the appeal against this judgment was completed and pending final decision.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Previous explorers were INCO and Kaiser Engineers.
Geology	Deposit type, geological setting and style of mineralisation.	Wet tropical laterite. In-situ chemical weathering of the ultramafic rocks.



Criteria	JORC Code explanation	Commentary
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all material drill holes: • easting and northing of the drill hole collar • elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar • dip and azimuth of the hole • down hole length and interception depth • hole length. If the exclusion of this information is justified on the basis that the information is not material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Axiom previously completed diamond coring using HQ and NQ triple tube to maximise recoveries within the mineralised horizons. The current program employs NQ single tube with tungsten carbide bit, having the same high level of recoveries. The previous program twinned Kaiser and INCO test pits, auger holes and the mined area. All collars are surveyed using handheld GPS recorded on UTM grid WGS84-57S with up to 5.0m accuracy. Collar elevation is recorded on RL. Drill holes are logged using logging forms. Relevant hole information such as final depth (EOH), core recovery, sampling interval, sample number, physical description, geological boundaries, lithology and mineralisation and alteration are noted.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated.	Only length weighting has been applied to reporting for the program. Assay intervals are generally undertaken on 1.0m regular intervals. The intervals are adjusted to geological boundaries with intervals ranging 0.3m minimum to 1.25m maximum. There are no outlier values requiring adjustment. An initial 0.6% cut-off is used to define mineralised nickel laterite envelopes. This was also used as the basis for previous Kaiser resource modelling. A second higher grade 1.2% Ni cut-off combined with the geological data is also used to provide higher grade intercepts more appropriate to some direct shipping requirements.
Relationship between minerali- sation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	The laterite is thin but laterally extensive. The intercepts are almost perpendicular to the mineralisation. The reported drill holes are located along secondary and tertiary ridge lines and along its slopes.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	See figures 1 to 3 and Table 1.



Criteria	JORC Code explanation	Commentary
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both low and higher grade intercepts are reported with corresponding thickness.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Both INCO and Kaiser Engineers undertook circa 6000 drill holes and pits, feasibility studies and economic analysis. Most of these studies were conducted prior to the establishment of the JORC Code.
Further work	The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Ongoing testing includes a focus on increasing the resource base by testing other known laterite areas within the tenement.

ENDS

About Axiom Mining Limited

Axiom Mining Limited focuses on tapping into the resource potential within the mineral-rich Pacific Rim. Through dedication to forging strong bonds and relationships with the local communities and governments where we operate, Axiom Mining has built a diversified portfolio of exploration tenements in the Asia Pacific region. This includes a majority interest in the Isabel Nickel Project in the Solomon Islands and highly prospective gold, silver and copper tenements in North Queensland, Australia. The Company is listed on the ASX. For more information on Axiom Mining, please visit www.axiom-mining.com

Competent Person's Statement

The information in this announcement that relates to Exploration Results is based on information compiled by Mr Jovenal Gonzalez Jr who is a Member of the Australasian Institute of Mining and Metallurgy (AuslMM). Mr Gonzalez has sufficient experience that is relevant to the styles of mineralisation and types of deposit under consideration and to the activity that is being undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves.' Mr Gonzalez is an employee to Axiom Mining Limited and consents to the inclusion in this report of the matters based on his information in the form and context in which it appears.

Disclaime

Statements in this document that are forward-looking and involve numerous risk and uncertainties that could cause actual results to differ materially from expected results are based on the Company's current beliefs and assumptions regarding a large number of factors affecting its business, including litigation outcomes in the Solomon Islands Court of Appeal. There can be no assurance that (i) the Company has correctly measured or identified all of the factors affecting its business or their extent or likely impact; (ii) the publicly available information with respect to these factors on which the Company's analysis is based is complete or accurate; (iii) the Company's analysis is correct; or (iv) the Company's strategy, which is based in part on this analysis, will be successful.